

Hydrogeological Assessment, 1066 Syer Line, Fraserville, ON

October 15, 2021

Prepared for: Township of Cavan Monaghan

Cambium Reference: 12971-002

CAMBIUM INC.

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1.0 Introduction

Cambium Inc. (Cambium) was retained by Township of Cavan Monaghan (Client) to complete a hydrogeological assessment in support of proposed land use changes at 1066 Syer Line, Fraserville, ON (Site) from agricultural to employment to allow for alternative uses on the property.

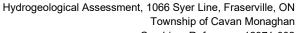
This hydrogeological assessment was completed in support of the proposed land use change and includes a general review of available geological / hydrogeological information, installation of two (2) new supply wells, 6-hour pumping tests at each new well, and water quality analysis of the supply water in accordance with the Ministry of the Environment and Climate Change (MECP) guideline D-5-5, specifically Section 4.4. Additionally, adjacent property owners within 500 m of the site were given the opportunity to have their well monitored during each pumping test.

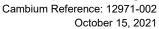
As part of the scope of work, Cambium was also retained to complete an environmental impact study (EIS) which was provided under a separate cover (Cambium Inc., 2021)

1.1 Site Description

The Site is roughly triangular and is approximately 34 hectares (~84 acres). The Site is mainly open fields and contains a watercourse that is designated as a natural linkage (NL) by the County of Peterborough (County) which runs through the southeastern corner of the Site and flows northeast off-site.

The Site is currently built upon with a vacant residence, two barns, two silos, and several small storage structures; the existing development is provided water and wastewater servicing by private on-site systems. The Site is designated as a Countryside Area as per Section 5 of the Official Plan for the Township of Cavan Monaghan ((Cavan Monaghan, 2013); the Site is outside of the boundaries of the Oak Ridges Moraine Plan Area. The current zoning at the Site is mainly Agricultural (A) with a portion of the southeast corner zoned at Natural Linkage (NL) where an unnamed watercourse flows northeasterly across the Site, and the very northwestern portion is also zoned NL. The Site is bordered by Syer Line to the south, rural residential (RR)







and rural employment (M2) to the west, Ontario Highway 115 to the north, and RR and A to the east. Additionally, the east of the Site, the area surrounding the unnamed waterbody is zoned as NL and Natural Core (NC). The proposed re-zoning at the Site would have the zoning of the Site change to M2.

An existing site plan is included in Figure 1 and additional land information is included in Appendix A.



2.0 Methodology

This section outlines the methodology followed to complete the hydrogeological assessment.

2.1 Well Installation

Cambium, on behalf of the Client, retained the services of Lone Star Drilling & Elevator Caisson Ltd. to install the two supply wells.

2.1.1 Well 1

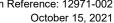
Well 1 (MECP Tag # A323405) was installed approximately 35 m north of the northeastern corner of the existing residential dwelling on July 06, 2021. Well 1 was installed to a depth of 33.53 mbgs, with an open bedrock hole extending from 28.85 mbgs to 33.53 mbgs. Well 1 was chlorinated upon completion. During installation, sediments described as coarsening down sequences of sand were encountered from ground surface to a depth of 14.33 mbgs, underlain by sandy till to 22.86 mbgs. A water-bearing gravel layer was encountered between 22.86 mgbs to 24.99 mbgs, underlain by a dense silty gravel till to 28.35 mbgs. Below the basal till, limestone bedrock was encountered and continued until the well termination at 33.53 mbgs.

The well driller's recommended pumping rate was 36 L/min.

The coordinates of Well 1 are UTM Zone 17 T and 703595 mE / 4896550 mN. The ground elevation at PW1 is 210 metres above sea level (masl). The top of casing of PW1 was determined to be 211 masl. The wellhead stickup of PW1 is 1.17 m. The well record of Well 1 will be forwarded to the Township once received from the Driller. The location of Well 1 is provided on Figure 1.

2.1.2 Well 2

Well 2 (MECP Tag # A323403) was installed approximately 12 m east of Well 1 on July 07, 2021. Well 2 was installed to a depth of 24.99 mbgs, with the screen extending from 22.86 mbgs to 24.99 mbgs. Well 2 was chlorinated upon completion. The stratigraphy of the sediment is the same as Well 1 and terminates in the dense gravel till at 28.35 mbgs.





The well driller's recommended pumping rate was 90 L/min. The coordinates of Well 2 are Zone 17 T and 703608 mE / 4896557 mN. The ground elevation at PW1 was 210 metres above sea level (masl). The top of casing of PW1 was determined to be 211 masl. The wellhead stickup of PW1 is 1.14 m. The well record of Well 2 will be forwarded to the Township once received from the Driller. The location of Well 2 is provided on Figure 1.

2.2 Groundwater Monitoring Network

The Client owns the property at 1256 Syer Line, which includes an abandoned dwelling. The supply well that services this property was included in the pumping test monitoring program. The location of this off-site well included in the monitoring network is outlined on Figure 2.

Pumping Test

2.2.1 Well 1

The pumping test of Well 1 commenced on July 19, 2021 at 9:25 and ceased the same day at 15:42 (a total of 6+ hours). The pump was installed to a depth of approximately 23.50 mbgs. The water withdrawal rate was maintained at an average rate of 32.0 L/min. Discharge water was directed to open field to the south of the vacant residential dwelling.

The water level of Well 1 was monitored at pre-determined time intervals for the duration of the pumping test using Solinst water level tape. Throughout the pumping test, the water levels of Well 2 and the existing on-site dug well were monitored. The water level of the off-site supply well at 1256 Syer Line was also monitored for the duration of the pumping test with a Solinst pressure transducer level logger.

A groundwater sample was collected from the discharge of Well 1 at 15:25 on July 19, 2021 and sent to SGS Canada Inc. in Lakefield (SGS) for analysis. The groundwater sample was analyzed for general organic and inorganic chemistry (including bacterial analyses). The concentration of free chlorine in water discharged from Well 1 was determined to be below detectable limits prior to sampling.

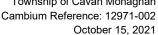


2.2.2 Well 2

The pumping test of Well 2 commenced on July 15, 2021 at 10:55 and ceased the same day at 16:56 (a total of 6 hours). The pump was installed to a depth of approximately 25.35 mbgs. The water withdrawal rate was maintained at an average rate of 82.5 L/min. Discharge water was directed to the open field south of the well to the east of the vacant residential dwelling.

The water level of Well 2 was monitored for the duration of the pumping test using Solinst water level tape. Throughout the pumping test, the water levels of Well 1 and the existing onsite dug well were monitored. The water levels of the off-site supply well were also monitored for the duration of the pumping test with a Solinst pressure transducer level logger.

A groundwater sample was collected from the discharge of Well 2 at 16:30 on July 15, 2021 and sent to SGS for analysis. The groundwater sample was analyzed for general organic and inorganic chemistry (including bacterial analyses). The concentration of free chlorine in water discharged from Well 2 was determined to be below detectable limits prior to sampling.





3.0 Geological and Hydrogeological Setting

The Site exhibits a gently rolling hilly topography, with the highest elevation being approximately 210 metre above sea level (masl) where the vacant dwelling and newly installed supply wells are located, and a gentle downwards slope in all directions from the built-up area.

The Site is located within the Cavan Creek subwatershed, a component of the Otonabee Region Watershed. Surface water drainage for the majority of the property drains towards the unnamed watercourse in the southeastern corner of the Site, which flows northeast off-site; however, surface water to the north of the vacant dwelling flows northeastward towards a wetland just off-site to the northeast. All surface water ultimately discharges into Cavan Creek approximately 3km northeast of the Site.

The Site is located in the physiographic region known as the Peterborough Drumlin Field. The Peterborough Drumlin Field is approximately 4,530 km² and extends from Hastings County in the east to Simcoe County in the west. This physiographic region contains approximately 3,000 drumlins in addition to many other drumlinoid hills and surface flutings of the till sheet. In general, the drumlins are composed of sand, gravel and boulder till and are separated by lowlying wetlands areas composed of fine-grained soils (Chapman, L.J. and D.F. Putnam, 1984).

According to Miscellaneous Release – Data 128 from the Ontario Geological Survey (Ontario Geological Survey, 2010) the following overburden and soils are located in the in the area of the Site:

- Course-grained glaciolacustrine deposits foreshore and basinal deposits
- Modern alluvial deposits clay, silt, sand, gravel, may contain organic remains

Recent updates to the local sedimentology indicate that the unit encountered at the surface is likely recent reworked lacustrine deposits (sediments originally laid down during glacial advance that were disturbed by meltwaters and sorted prior to redistribution as "reworked lacustrine deposits", typically resulting in the removal of finer sediments from the underlying till) from the recession of the last glaciation. The underlying units correspond to Newmarket Till, a sandy till as described in literature, with layers of sorted sediments formed in glacial meltwater



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channels known as valley infill sediments or Inter-Newmarket Sediments (INS). These valleys were incised in to the Newmarket till under glacial lobes and extreme water pressures, and later buried by more recent sediments and glacial advances. These INS formations are thought to be the source of the highly productive well at 1256 Syer Line, and although they can be regionally extensive, their locations are difficult to anticipate. Well 2 is interpreted to be screened across one such feature, albeit much less productive and not likely hydraulically connected to the more productive INS feature screened in the test well at 1256 Syer Line. That said, there is a potential that other areas on the site could encounter a thicker and more productive INS feature. Recent interpretations indicate these are typically located in low lying areas near steep sided valley walls or one sided valleys represented by highlands adjacent to lowlands. Following these assumptions, additional INS features would be more prominent in the low lands adjacent to the onsite drainage features.

According to Miscellaneous Release – Data 219 from the Ontario Geological Survey (Ontario Geological Survey, 2007), the bedrock in the area of the Site consists of Middle Ordovician rocks from the Simcoe Group. The Site is composed of nodular and black laminated limestone of the Lindsay Formation. This bedrock formation is not typically a high yielding water bearing host and known locally for poorer quality (aesthetically) groundwater containing increased iron and sulphur concentrations that affect colour and taste.

3.1 Water Well Records

The Ministry of Environment Conservation and Parks (MECP) Water Well Information System (WWIS) was accessed to review water well records in the area of the Site. There were nine water well records located within approximately 500 m of the Site (Figure 3). The following water well records were identified:

- Eight (8) water well records for drilled wells
- One (1) water well records for a dug well existing well on Site

As per the MECP records, the soil profile generally consisted of >1 m of topsoil, underlain by grey to brown sandy clay, sometimes combined with gravel; periodic solely clay and solely gravel layers were also reported. Two (2) of the drilled wells were advanced into bedrock



composed of limestone; the bedrock contact was found approximately 22 mbgs. Bedrock continued until well termination. Water bearing sediments were identified within overburden between 6.7 to 68.6 mbgs, averaging 22.3 mbgs. Water bearing strata were also identified within 2 m below the overburden – bedrock contact. The depth of the bedrock contact and description of overburden provided by the well records was similar to the conditions encountered on-site as part of well installation at Site.

The average static water level of the drilled wells was 7.75 mbgs, and static water level of the dug well was 5.49 mbgs. The recommended flow rate ranged from 4 gallon per minute (gpm, assumed to be US gallons per minute) to 12 gpm, averaging 7 gpm. Further information summarized from the water well records are listed below in Table 1.

Table 1 Water Well Record Information

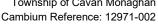
		Total Depth (mbgs)	Depth Water Encountered (m)	Depth Installed into Bedrock (m)	Static Water Level (mbgs)	Recommended Pumping Rate (gpm)
Drilled	Min	12.59	10.06	1.22	0.00	5.00
Wells	Max	68.58	68.58	1.83	30.48	12.00
Count:8	Avg.	25.19	24.1	1.52	7.75	7.38
Dug Wells	Min	6.71	6.71	-	5.49	4.00
Count:1	Max	6.71	6.71	-	5.49	4.00
	Avg.	6.71	6.71	-	5.49	4.00

Water well record 5117898 was plotted to the north of the vacant dwelling on-Site. This record indicates the well was installed to a depth of approximately 6.71 mbgs in brown sand. This well was observed during Cambium's Site visits and was monitored for the duration of the pumping tests.

3.2 Vulnerable and Regulated Areas

As per the Ministry of the Environment, Conservation and Parks (Ministry) Source Water Protection Information Atlas (SPIA) the Site is within the following areas:

- Significant Groundwater Recharge Area (SGRA)
- Highly Vulnerable Aquifer (HVA)
- Intake Protection Zone 3 (IPZ-3)





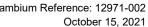
These delineations could influence the type of development and or construction practices for future developments as follows:

SGRAs exist where water from surface more easily infiltrates the ground to recharge an aquifer that is used for municipal or other drinking water supplies. An SGRA helps maintain the water level in an aquifer that supplied drinking water (including private wells) and has a higher than average recharge comparatively across the Source Protection Area. Any future development at the Site will have to ensure that the post-development water balance maintains an acceptable amount of impervious area to allow for infiltration of surface water into the SGRA. If impervious areas are reduced due to development, groundwater recharge should be maintained through the implementation of LID measures, such as enhanced infiltration, where practicable.

HVAs are aquifers that are more sensitive to contamination. This should be taken into account for the proposed development. If the groundwater or surface water will be affected by the construction or day-to-day activities of a future development, the stormwater and dewatering discharge may need to be treated before it can return to the natural surface water / groundwater receiver.

An IPZ-3 is an area of land and water around a municipal intake pipe that contributes source water to a drinking system. The zone 3 designation means that contaminants could reach the intake of a Municipal Drinking Water System and after a large storm. As with the HVA requirements, contaminated groundwater and surface water from the development may have to be treated prior to reaching the natural receiver.

The Site is located within regulated areas, as per Otonabee Region Conservation Authority (ORCA) information and therefore any development at the Site would require submission to the ORCA prior to commencement. The SPIA mapping is updated as necessary and available at www.swpip.ca.

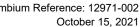




3.3 Hydrogeological Conditions

Based off of the wells drilled for this work program, the shallow overburden sediment at Site is sandy to 14.3 mbgs where it is underlain by dry, sandy till to 22.9 mbgs and a gravel water bearing unit to 28.3 mbgs, where bedrock was encountered. Based off information from the MECP WWIS and installation of the wells for this work program, three aquifers exist on site. The upper unit is an unconfined sand unit that will likely produce in the range of 100L/min. during well advancement the drilling was paused to allow a rough estimate of yield and quality at 14m depth. This unit wasn't screened during this program, however the onsite dug well likely just penetrated the top of this unconfined unit. The upper unit appeared clearer with less suspended sediment than the two deeper units, however would be more susceptible to drought conditions and surface contamination. The second or middle unit is a confined, overburden aquifer that occurs within a gravel layer between 22.86 mgbs to 24.99 mbgs and represents sediments reworked under glacial pressures and melt water within the overall sandy till unit (Newmarket Till). This unit has a cloudy appearance owing to the silt content in the host till deposit where these channel infill sediments were incised. The deeper unit is a bedrock contact aguifer that occurs at, or just below, the overburden – bedrock contact. The connectivity of the middle overburden aquifer and the deeper aquifer systems was not apparent from drilling. However, it is likely that there is some degree of hydraulic connection between the shallow overburden aguifer and the underlying bedrock aguifer given the pumping responses observed in the wells when the.

Shallow unconfined groundwater flow is assumed to follow the overlying topography at Site. It is assumed that the unconfined overburden groundwater discharges to surface and therefore will ultimately flow eastwards to Cavan Creek as discussed in Section 3.0. The onsite deeper groundwater flow was not available from onsite information but typically flows towards regional discharge locations in this case the Ottonabee River to the east.





4.0 Results

This section presents the results of the pumping tests and the groundwater quality comparison against parameters outlined by the Ontario Drinking Water Quality Standard (ODWQS)

4.1.1 Well 1

The static water level of Well 1 was 5.91 mtop (which corresponds to a depth of 4.74 mbgs) just prior to the pumping test. The pumping test commenced at 9:25 am on July 19, 2021 at a rate of 32 Litres per minute (L/min). Within 10 minutes after the commencement of the pumping test, the water level of PW1 lowered to 9.74 mtop. After the initial 10-minute interval the water level of Well 1 lowered consistently until the end of the pumping test to a level of 11.89 mtop. The depth of drawdown achieved at Well 1 upon completion of the pumping test was 5.98 m (at 3:38 pm on July 19, 2021). The pumping rate was maintained at an average rate of 32 L/min throughout the test, which equated to approximately 11,520 L of water withdrawn within a 6-hour period. The Specific Capacity of Well 1 during this 6-hour pumping test was calculated to be 5.35 L/min/m. The theoretical yield of well 1, given a probable intake of 32m and a static level of 5.9m allows for 26.1 m of drawdown, is 139 L/min.

Upon completion of the pumping test the water level of Well 1 was allowed to recover. By 4:52 pm on July 19, 2021 the water level in Well 1 recovered to 6.37 mtop (or 92% recovery to pretest static conditions). The water level responses of Well 1 during the pumping test are provided on a time/drawdown plot in Figure 4.

The drawdown data recorded from Well 1 were imported into AquiferTest Pro[™] and processed to determined transmissivity and hydraulic conductivity.

The transmissivity was calculated to be 50 m²/day; the hydraulic conductivity was 2.70×10^{-4} m/s. The results of the aquifer test analyses are outlined below in Table 2. The AquiferTest ProTM results are included in Appendix C.



4.1.2 Well 2

The static water level of Well 2 was 5.60 mtop (which corresponds to a depth of 4.46 mbgs) just prior to the pumping test. The pumping test commenced at 10:55 am on July 15, 2021 at a rate of 82.5 L/min. Within 10 minutes after the commencement of the pumping test, the water level of PW1 lowered to 11.09 mtop. After the initial 10-minute interval the water level of Well 2 lowered consistently until the end of the pumping test to a level of 20.84 mtop. The depth of drawdown achieved at Well 2 upon completion of the pumping test was 15.24 m (at 4:55 pm on July 15, 2021). The pumping rate was maintained at an average rate of 82.5 L/min throughout the test, which equated to approximately 29,700 L of water withdrawn within a 6hour period. The Specific Capacity of Well 2 during this 6-hour pumping test was calculated to be 5.41 L/min/m. The theoretical yield of well 2, given a probable intake of 23 m and a static level of 5.6 m allows for 26.1 m of drawdown, is 94 L/min.

Upon completion of the pumping test the water level of Well 2 was allowed to recover. By 5:55 pm on July 15, 2021 the water level in Well 2 recovered to 8.76 mtop (or 79% recovery to pretest static conditions). The water level responses of Well 2 during the pumping test are provided on a time/drawdown plot in Figure 5.

The drawdown data recorded from Well 2 were imported into AquiferTest ProTM and processed to determined transmissivity and hydraulic conductivity.

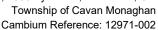
The transmissivity was calculated to be 7 m²/day; the hydraulic conductivity was 1.65 x 10⁻⁵ m/s. The results of the aquifer test analyses are outlined below in Table 2. The AquiferTest Pro[™] results are included in Appendix C.

Table 2: Aquifer Test Pro Results

Well	Transmissivity (m²/day)	Hydraulic Conductivity (m/s)
Well 1	50	2.70 x 10 ⁻⁴
Well 2	7	1.65 x 10 ⁻⁵

4.2 Surrounding Well Influences

The water level of the two other on-Site supply wells were monitored during each pumping test. The existing dug well on-Site (Well Record # 5117898) exhibited no influence during





either of the pumping tests; the water level remained static at 4.92 mtop (which corresponds to a depth of 4.98 mbgs)

Well 2 showed a minor influence during the pumping test for Well 1. The total influence at Well 2 during this time was a maximum drawdown of 0.32 m, which is considered a negligible amount.

Well 1 showed a significant influence during the pumping test for Well 2. The total influence at Well 2 during pumping of Well 1 was a maximum drawdown of 5.18 m, which is comparable to the amount of drawdown exhibited during the actual pumping test for Well 1 (5.98 m).

The total fluctuation observed at the well located at 1256 Syer line did not exceed 5 cm during either pump test, there was no observed influence at this well which was located 1.5 km to the east.

The observed interference indicates the intermediate aguifer is hydraulically connected to the bedrock interface aguifer, this was not unexpected as the vertical separation between the two water bearing units was only 3.6 m. The upper unconfined aguifer appears to be hydraulically isolated from the lower two aquifers, and as such both aquifers could be pumped simultaneously where needed.

Water level fluctuations are included in a time/water level hydrograph on Figure 4 and Figure 5.

4.3 Extrapolated Drawdown

The water levels recorded near the end of the pumping test (when a stable lowering was recorded) were extrapolated to 1 year and 20 years on a logarithmic time scale. This approach assumed that a pumping rate of 32.0 L/min is maintained continuously during a 1 year and 20-year period for Well 1 and a pumping rate of 82.5 L/min is maintained continuously during a 1 year and 20-year period for Well 2. This kind of assessment is valuable in estimating long-term impacts related to water withdrawal at a well.



Table 3: Results of Drawdown Extrapolation

Well	Time Frame	Extrapolated Drawdown (m)	Available Drawdown (m)
	Beginning of Test	-	23.09
Well 1	End of Test	5.98	17.11
vven	1 Year	8.34	14.75
	20 Years	10.09	13.00
	Beginning of Test	-	17.55
Well 2	End of Test	15.24	2.31
vven z	1 Year	35.04	N/A
	20 Years	45.65	N/A

Note: Extrapolated drawdown indicates the expected drawdown from the static water level of each respective well

The results of the extrapolated drawdown analysis assume that if the constant water withdrawal observed during the pumping test continued indefinitely, the depths of drawdown would be estimated to be 8.34 m after 1 year of constant pumping, and 10.09 m after 20 years of constant pumping. The corresponding depths of available drawdown for the 1- and 20-year periods would be estimated to be 14.75 m and 13.00 m, respectively. For Well 2, it was clear from the extrapolated drawdown analysis that the pumping rate (82.5 L/min) was unsustainable for any period longer than 6 hours. The estimated depths of available drawdown after sustained pumping are considered to be suitable for a water supply at Well 1. For Well 2, a lower recommended pumping rate similar to that of Well 1 should be considered for a sustainable long-term pumping rate.

4.4 Vertical Gradient

The vertical difference between the two water bearing zones (intermediate and bedrock interface) indicate a slight downward gradient. This suggests that migration of waters and any dissolved contaminant would migrate downwards from the intermediate to the deeper aquifer.

4.5 Groundwater Quality

A groundwater sample was collected from Well 1 and Well 2 near the end of each respective pumping test; these samples were analysed for general organic and inorganic chemistry,



including bacteria analysis. Duplicate samples of each well were collected for bacteria analysis.

The water sample at Well 1 was collected just prior to the end of the pumping test at 3:20 pm on February 19, 2021 and the water sample at Well 2 was collected just prior to the end of the pumping test at 4:25 pm on February 15, 2021. Field observations noted that the water sampled from both wells was cloudy and opaque with no odour; sediment remained permanently in suspension. Field parameters were analysed for in the field and are summarized in Table 4.

Table 4: Water Quality Field Parameters

Well	Time	Oxidation-Reduction Potential (mV)	Conductivity (µS/cm)	рН	Temperature (°C)
Well 1	3:20 pm	132	420	8.56	16.1
Well 2	4:25 pm	125	350	8.04	17.1

Bolded values exceed ODWQS criteria

The groundwater samples were analysed by SGS and compared to the Ontario Drinking Water Quality Standard (ODWQS)(Ministry of Environment, 2006).

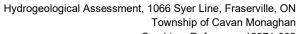
Water quality results are attached in Appendix D and exceedances are reported in Table 5:

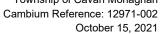
Table 5 Groundwater Quality

Parameter	Well 1	ODWQS (mg/L)
Hardness	113	100
Sodium	45.9	20
Total Coliform ¹	2	0
Parameter	Well 2	PWQO Criteria (mg/L)
Hardness	167	100

Exceedance report in the duplicate sample only

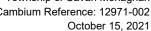
The pH exceedance reported in the field for pH at Well 1 was not reported during the lab analysis; pH is interpreted as being within ODWQS criteria for both wells. Total Coliform exceeded the ODWQS criteria in the duplicate sample at Well 1. Because there was no total coliform reported from the original Well 1 sample, it is interpreted that the exceedance associated with the duplicate is from field contamination while sampling. Hardness exceeded the ODWQS criteria at both Well 1 and Well 2 suggesting that drinking water from the supply wells should be treated for hardness with an ion exchange softener prior to use to avoid scale







buildup in plumbing and appliances. The suspended solids observed in both of the wells would require a filtration unit, though prolonged pumping should create an effective gravel pack as sediment is removed and source water should clear up with time.





5.0 **Conclusions and Recommendations**

Cambium completed a pumping test of the two newly installed wells at the Site. Well 1 was screened between depths of 28.35 mbgs to 33.53 mbgs and is considered to be installed in a confined bedrock contact aguifer that occurs immediately below the overburden – bedrock contact. Well 2 was screened between depths of 22.86 mbgs to 24.99 mbgs and is considered to be installed in a confined overburden aguifer that occurs between 22.86 mgbs to 24.99 mbgs. A third upper aquifer was encountered during drilling, and is partially penetrated by the onsite dug well, this well was observed to produce clear water at a rate of 100 L/min but was not isolated with a well for further testing during this campaign due to budgetary constraints.

Water withdrawal occurred for a continuous 6-hour period during both pumping tests; the rate for Well 1 was 32 L/min and the rate for Well 2 was 82.5 L/min. In total, 11,520 L and 29,700 L of water was withdrawn from the wells respectively. The Specific Capacity of Well 1 during the 6-hour pumping test was 5.35 L/min/m, and the Specific Capacity of Well 2 was 5.41 L/min/m, resulting in a theoretical yield of 139 L/min and 94 L/min respectively (the difference between them is a result of the available drawdown / depth). The proven continual pumping rate of 32L/min was observed when extrapolating drawdown in Well 1, Well 2 was pumped in excess of its maximum sustainable rate as was evidenced by the failure of this well to reach an equilibrated pumping level. While additional testing may indicate a higher combined yield, a maximum rate of 32L/min is appropriate for preliminary planning purposes from the intermediate and bedrock contact aquifer. The upper unconfined aquifer may not be present across the site in the thicknesses observed, however; where it is an additional 100L/min is available for future uses.

Upon completion of the pumping test for Well 1, approximately 11,520 L was pumped from the well and a maximum drawdown of 5.98 m was recorded (leaving approximately 17.11 m of available drawdown in the well). The Test Well was also pumped at a rate of 32 L/min for the entirety of the test. The extrapolated depths of drawdown indicated that the overburden aquifer should be able to sustain long-term water withdrawal. The time of year studied (midsummer) does not represent the peak of water table fluctuations, and the water level is



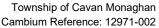
expected to rise in the spring months, further increasing the available drawdown in the well. As such, the groundwater resources available at Well 1 (i.e., overburden – bedrock contact aquifer) are considered to be suitable for industrial water supply.

Upon completion of the pumping test for Well 2, approximately 29,700 L was pumped from the well and a maximum drawdown of 15.24 m was recorded (leaving approximately 2.31 m of available drawdown in the well). The Test Well was also pumped at the peak demand rate of 82.5 L/min for the entirety of the test. While the tested rate was sustainable for the 6 hours, the steady decline in pumping levels indicate the well would not be able to sustain this rate for much longer and should be pumped at a lower rate (<50LPM) or deepened to include the bedrock contact aquifer to approach the upper theoretical yields of ~139L/min.

The Dug Well that was located near-by showed minimal to no response to the water withdrawal at the Test Well, as such no impacts to the groundwater users within 500 m (or further) from the Site who obtain water from the upper aquifer are anticipated upon the future development of the Site. There were no deeper wells identified within the MECP WWIS database within 500m of the site. Future testing for development specific wells should include off-site monitoring if available.

The results of the groundwater sampling indicated that turbidity, total coliforms and hardness exceeded their corresponding ODWQS criteria. Additionally, the total fraction of aluminum, iron and manganese exceeded the ODWQS criteria, however the dissolved fraction of these metals did not. Cambium recommends that the groundwater be treated with appropriate filtration and softened prior to use. Cambium also recommends that the grading plan ensure that run-off is conveyed away from the well and both onsite and adjacent septic systems are installed with the maximum amount of separation possible, particularly if sourcing the groundwater supply from the upper shallow aquifer.

Upon development of the Site, Well 1 and Well 2 could be used as water supply wells. The pump in Well 1 should be installed to a depth of 32 mtop and the pump at Well 2 should be installed to a depth of 23 mtop. The water level of both wells should be monitored to determine long term water withdrawal influences, monitoring frequencies should be accordant with the



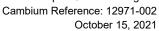


anticipated demand (i.e. more frequently where higher demands are anticipated). The depth of the pump should be adjusted as needed. An additional unconfined aquifer exists from surface to 14 m deep and should be considered for use prior to advancing to the deeper units, the unit may not be present across the site but where encountered has the potential to provide clear water. This unit would not likely require filtration but could require disinfection given the unconfined nature of the water bearing sediments and the potential for surface contaminants to migrate to the aquifer after development.

The proven extrapolated long term pumping rate of 32L/min or 46,000L/day is considered sustainable and appropriate for planning purposes in the absence of further testing. The choice of targeting one water bearing unit over the other would be a site based decision, however; the deeper unit would likely be a more practical choice, given the greater available drawdown and resulting yield.

As an example of future industrial development, a factory - excluding production or process water demands, requires 75 L/day/employee (factory without showers) or 125 L/day/employee (factory with showers). In other words, the perpetual pumping of the intermediate aguifer (Well 1), as tested at 32L/min (46,000L/day), could supply up to 613 employees without showers, or 368 with showers. Additional supply is available from the upper unconfined aquifer (on-site dug well) which could, given the limited observations during drilling advancement, support a water demand up to 100L/min or 144,000 L/day.

In summary, there is ample proven supply for industrial uses that do not require process or washing water across the site. There is an indicated additional and isolated supply potential from the upper unit which could support either non-process water industrial development, or industrial uses that require process water up to ~144,000L/day. Cambium recommends a further testing program to provide proven water quality and quantity from the upper unconfined aquifer as well as the occurrence of the upper unconfined aquifer across the site.





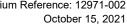
Cambium Inc.

Nicole Heikoop, M.Sc., GIT Technician Mike Bingham, P.Geo. Senior Project Manager/Hydrogeologist

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MEB/nmh

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6.0 References

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- Cambium Inc. (2021). Geotechnical Investigation Report 380 High Street, Collingwood, Ontario.
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- Ministry of Environment. (1996). *Procedure D-5-5, Technical Guideline For Private Wells:*Water Supple Assessment.
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Hydrogeological Assessment, 1066 Syer Line, Fraserville, ON Township of Cavan Monaghan

Cambium Reference: 12971-002

October 15, 2021

7.0 Standard Limitations

Limited Warranty

In performing work on behalf of a client, Cambium relies on its client to provide instructions on the scope of its retainer and, on that basis, Cambium determines the precise nature of the work to be performed. Cambium undertakes all work in accordance with applicable accepted industry practices and standards. Unless required under local laws, other than as expressly stated herein, no other warranties or conditions, either expressed or implied, are made regarding the services, work or reports provided.

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Site Assessments

A site assessment is created using data and information collected during the investigation of a site and based on conditions encountered at the time and particular locations at which fieldwork is conducted. The information, sample results and data collected represent the conditions only at the specific times at which and at those specific locations from which the information, samples and data were obtained and the information, sample results and data may vary at other locations and times. To the extent that Cambium's work or report considers any locations or times other than those from which information, sample results and data was specifically received, the work or report is based on a reasonable extrapolation from such information, sample results and data but the actual conditions encountered may vary from those extrapolations.

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Reliance

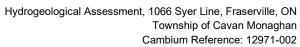
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Appended Figures
Appended Figures
Appended Figures
Appended Figures

EXISTING DUG WELL DRILLED **DRILLED** WELL 1 WELL 2

HYDROGEOLOGICAL INVESTIGATION

TOWNSHIP OF CAVAN-MONAGHAN

1066 Syer Line, Fraserville, Ontario

LEGEND

Drilled Well

Dug Well

Site (approximate)

Notes:

- Base mapping features are @ Queen's Printer of Ontario, 2019 (this does not constitute an endorsement by the Ministry of Natural Resources or the Ontario Government).

- Distances on this plan are in metres and can be converted to feet by dividing by 0.3048.

- Cambium Inc. makes every effort to ensure this map is free from errors but cannot be held responsible for any damages due to error or omissions. This map should not be used for navigation or legal purposes. It is intended for general reference use only.



194 Sophia Street Peterborough, Ontario, K9H 1E5 Tel: (705) 742.7900 _ Fax: (705) 742.7907

SITE PLAN

Project No.: August 2021 12971-002 Rev.: Scale: Projection: NAD 1983 UTM Zone 17N 1:5,000 Checked by: Created by: MAT MB

HYDROGEOLOGICAL INVESTIGATION

TOWNSHIP OF CAVAN-MONAGHAN

1066 Syer Line, Fraserville, Ontario

LEGEND

Drilled Well

Dug Well

1256 Syer Line

Site (approximate)

Notes:

- Base mapping features are @ Queen's Printer of Ontario, 2019 (this does not constitute an endorsement by the Ministry of Natural Resources or the Ontario Government).

- Distances on this plan are in metres and can be converted to feet by dividing by 0.3048.

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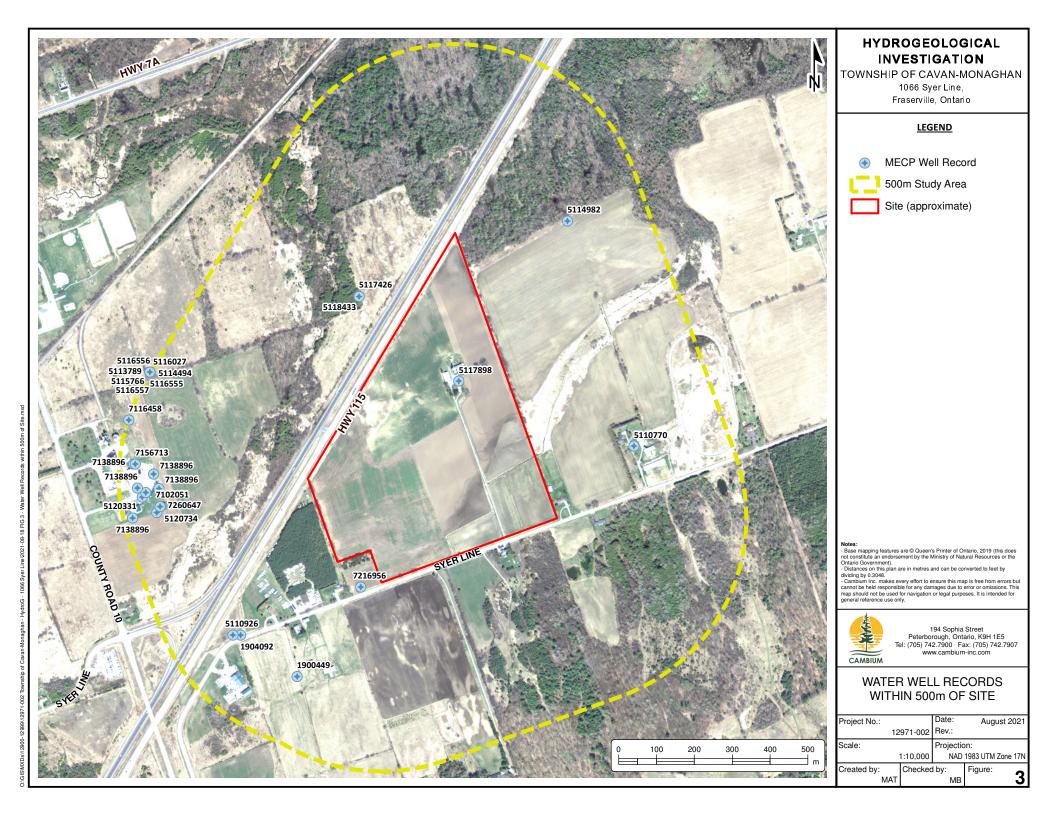


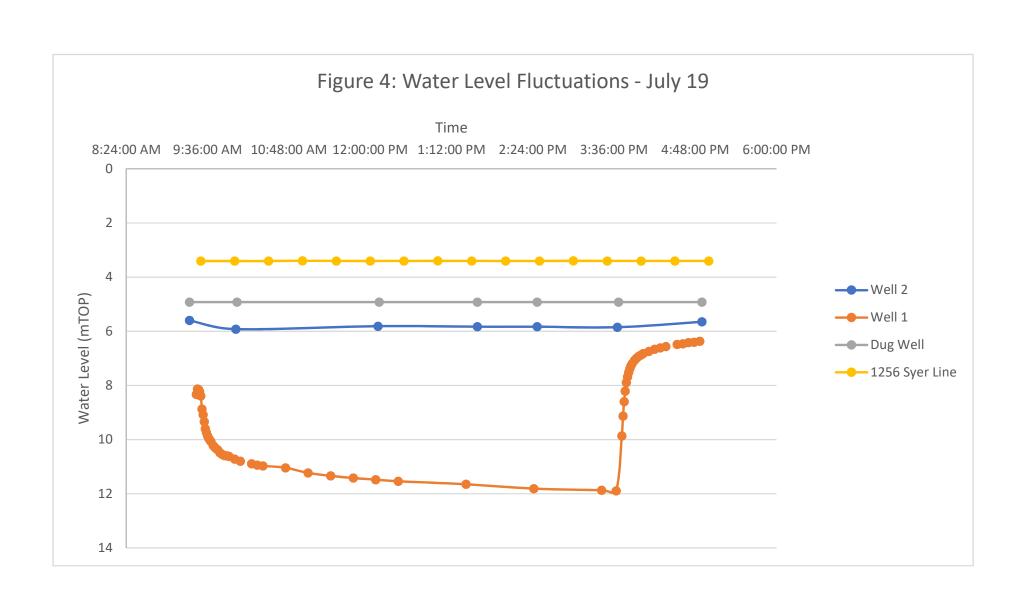
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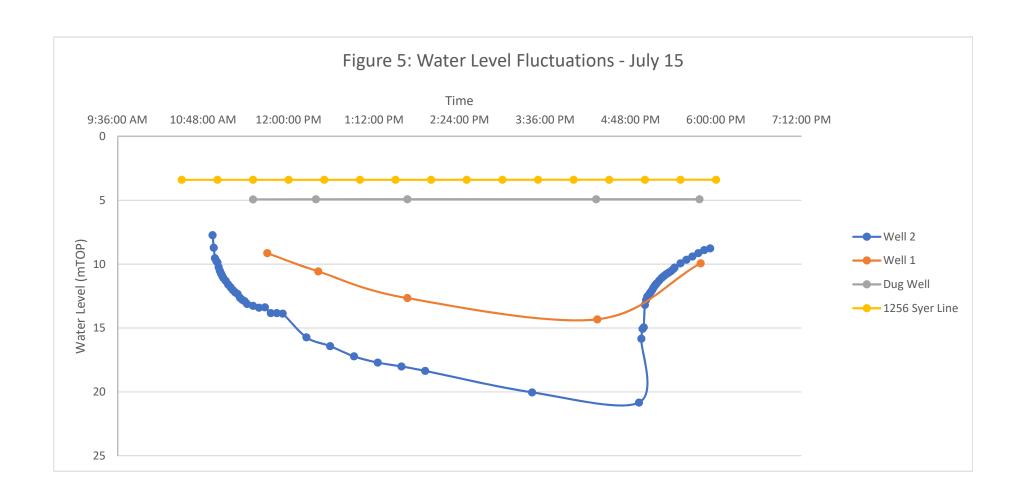
OFF-SITE GROUNDWATER MONITORING NETWORK

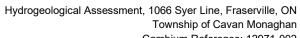
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Cambium Reference: 12971-002 October 15, 2021

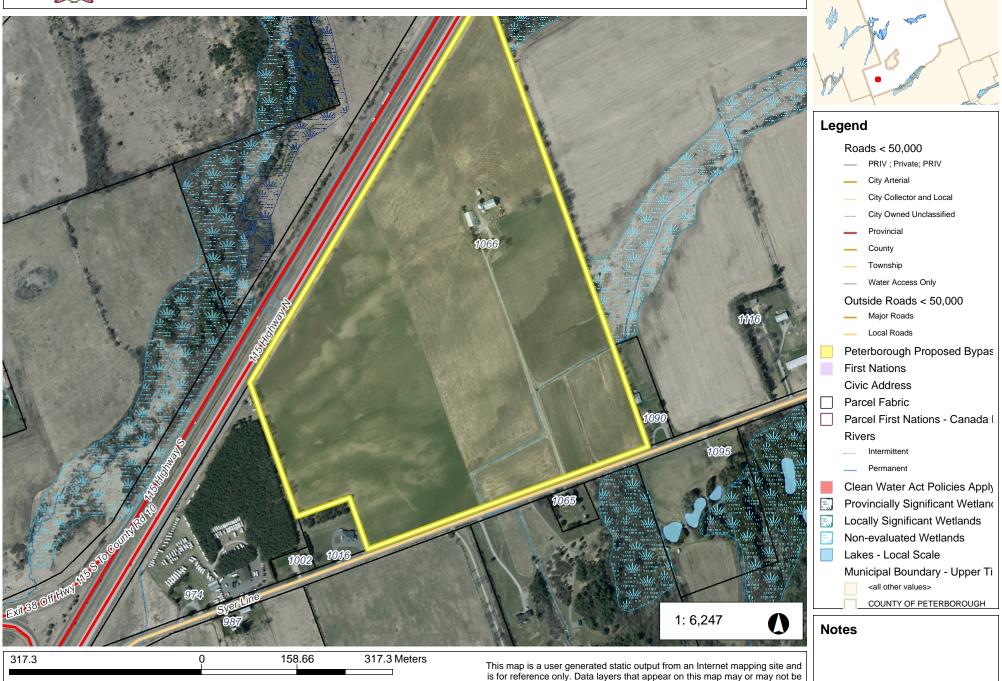
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© Latitude Geographics Group Ltd.

1066 Syer Line - Aerial

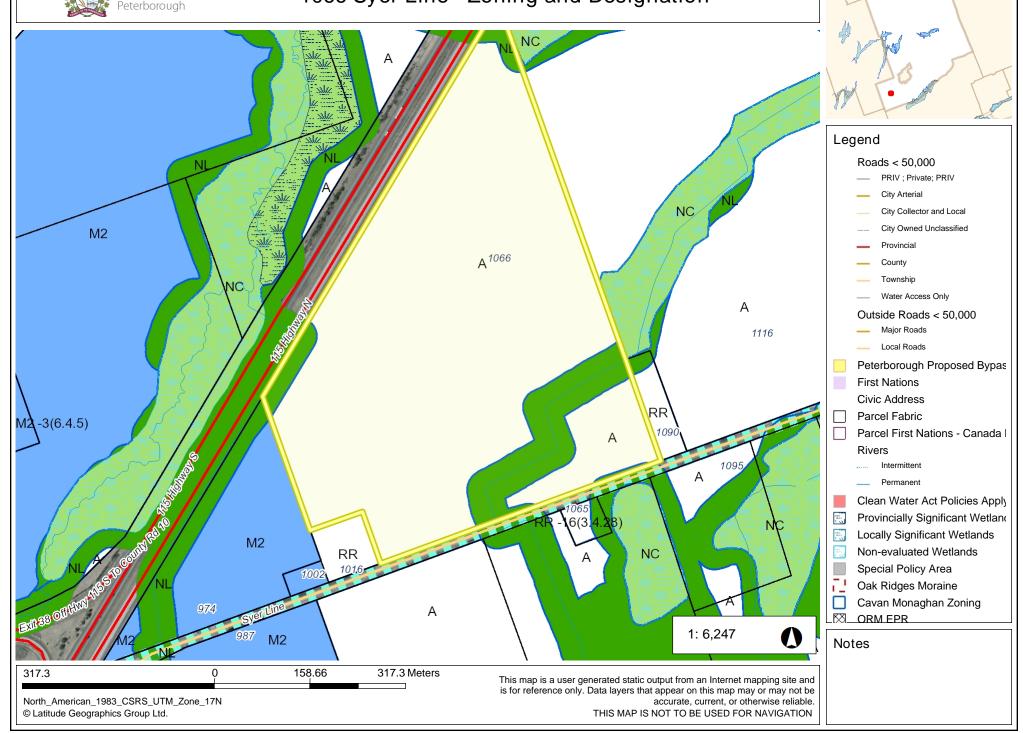


accurate, current, or otherwise reliable.

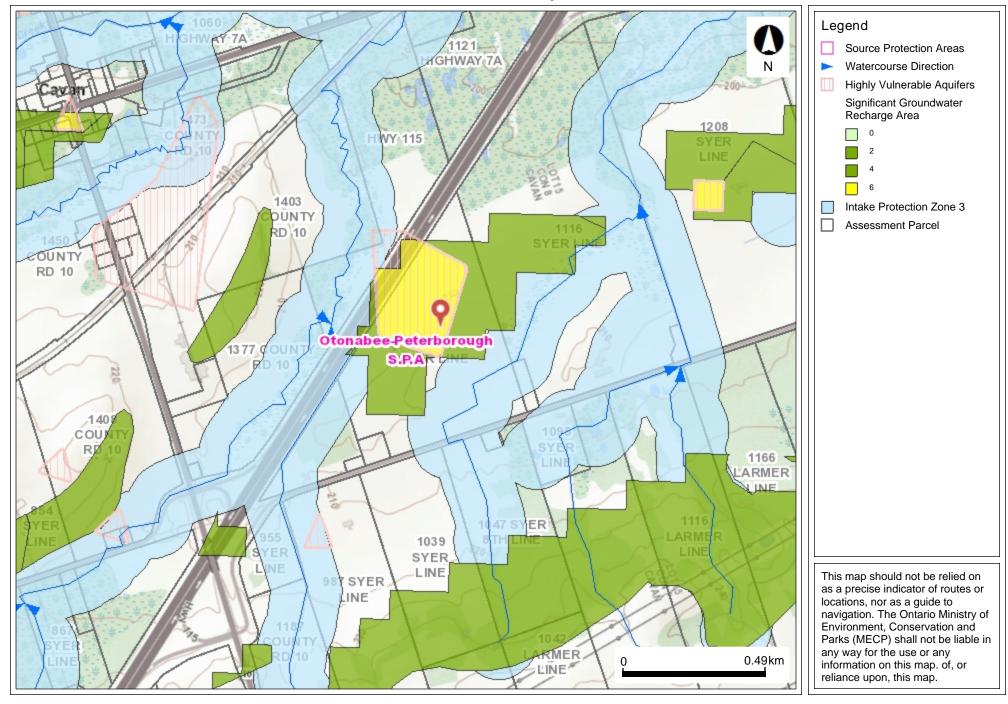
THIS MAP IS NOT TO BE USED FOR NAVIGATION



1066 Syer Line - Zoning and Designation



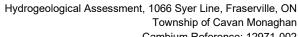
SPIA Map

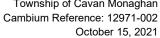




Map Created: 8/10/2021

Map Center: 44.19219 N, -78.45445 W







Appendix B Local Water Well Records

(New on-site well records to be provided when received)

The Ontario Water Resources Act WATER WELL RECORD

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	WELL CONT		CBOT	DAY -50	n/s 470	LICENCE NUMBER		DATA SOURCE DATE OF INSPECT	S8 CO	1921	1 16 LEO	5	33
ADDRESS					91.5	,,-,		DATE OF INSPECT	10#	INSPECTOR	1		
NAME OF	DRILLER OF		CAUK			LICENCE NUMBER	-	REMARKS:			e,	7	
SIGNATUR	25 E OF CONT	RACTOR	3 A Turi	<u> </u>	SUBMISSION DATE		-	OFFICE				SS	ES
1	111	Y OF T	12	VIRON	DAY 13 M		(1)	Ō				יממי	—4—77 FORM 7

The Ontario Water Resources Act 310 e WATER WELL RECORD

5110926 2. CHECK 🗵 CORRECT BOX WHERE APPLICABLE COUNTY OR DISTRICT TOWNSHIP, BOROUGH, CITY, TOWN 0700 LOG OF OVERBURDEN AND BEDROCK MATERIALS (SEE INSTRUCTIONS) MOST COMMON MATERIAL DEPTH - FEET OTHER MATERIALS GENERAL DESCRIPTION 50 SHLAY CLAY 0 SHOWN 50 70 VERYFII SHND INHIER 70 75 TREY TRAVELLY SHAKE 81 TREY LIMESTONE (31) 0.9506(0581) | 0.070 | 0890 | 0.07.521.7172 | 0.08.12.15 | | | | | | | | | 32 41) WATER RECORD (51) **CASING & OPEN HOLE RECORD** SCREEN KIND OF WATER DEPTH TO TOP 2 SALTY 4 MINERAL **180** 2 [] GALVANIZED 010075 188 CONCRETE **PLUGGING & SEALING RECORD** 4 OPEN HOLE DEPTH SET AT - FEET MATERIAL AND TYPE (CEMENT GROUT LEAD PACKER, ETC ☐ STEEL 1 | FRESH 3 | SULPHUR
2 | SALTY 4 | MINERAL ² ☐ GALVANIZED

3 ☐ CONCRETE 1 FRESH 3 SULPHUR
2 SALTY 4 MINERAL OPEN HOLE 27.1 1 STEEL Z 🗌 GALVANIZED 1 | FRESH 3 | SULPHUR
2 | SALTY 4 | MINERAL 30-33 CONCRETE OPEN HOLE LOCATION OF WELL 02 15-16 30 17-18 HOURS 30 MINS 00/2 1 D PUMP 2 BAILER IN DIAGRAM BELOW SHOW DISTANCES OF WELL FROM ROAD AND LOT LINE INDICATE NORTH BY ARROW. PUMPING
RECOVERY O 2 See O 2 28 SI FEET 45 MINUTES 60 MINUTES 0 2353 FEET 0 2353 FEET PUMP INTARA SET AT SET OF SET RECOMMENDED PUMP TYPE MILLEKOOK SHALLOW DEEP 1 TW WATER SUPPLY S ABANDONED, INSUFFICIENT SUPPLY
B ABANDONED, POOR QUALITY FINAL STATUS 3 | TEST HOLE 7 UNFINISHED OF WELL 4 | RECHARGE WELL DOMESTIC
STOCK
INRIGATION 6 MUNICIPAL ZINE CHIVINIV WATER 4 | INDUSTRIAL USE OI COOLING OR AIR CONDITIONING

NOT USED ☐ OTHER well CABLE TOOL
ROTARY (CONVENTIONAL)
ROTARY (REVERSE) 6 | BORING
7 | DIAMOND METHOD OF ■ □ IETTING DRILLING DRILLERS REMARKS 1/88 S AIR PERCUSSION DATA ONLY 4923 4923 WELL DRILLING CONTRACTOR OFFICE USE 4923 CSS.ES

The Ontario Water Resources Act WATER WELL RECORD

Print only in spaces provided. Municipality 5117426 Mark correct box with a checkmark, where applicable 11 51024 CON Con block tract survey, etc. Lot Township/Borough/City/Town/Village County or District Plan 117 Cavan 48-53 Address **9.7** Cavan , Ontario iii Elevation RC Basin Code للل LOG OF OVERBURDEN AND BEDROCK MATERIALS (see instructions) Depth - feet General description Other materials General colour Most common material From 0 2 Soft Brown Top Soil 18 2 Packed Stones Clay Brown 73 18 Cemented Hard Pan Grey 73 75 Loose Gravel & Water Brown 31 32 CASING & OPEN HOLE RECORD WATER RECORD 51 Inside diam inches Depth - feet Water found Kind of water inches То Steel ::
Galvanized
Concrete
Open hole From Depth at top of screen 30 Sulphur Minerals Gas Fresh ☐ Salty Sulphur Minerals Gas ₁ □ Fresh 188 0 75 PLUGGING & SEALING RECORD 6-1 intested Salty Steel Galvanized Concrete Open hole Plastic Annular space Sulphur Minerals Gas ☐ Fresh Depth set at - feet Material and type (Cement grout, bentonite, etc.) ☐ Salty То From Sulphur Minerals Gas ☐ Fresh 15 Bentonite (Holeplug) 0 ☐ Salty Steel Galvanized Concrete Open hole Plastic ₁ ☐ Fresh 。

Salty Duration of pumping

GPM 2...... Hours Pumping test method Pumping rate LOCATION OF WELL ..3 **Q**iểs 10 in diagram below show distances of well from road and lot line. Pumping Static level Water levels during Indicate north by arrow. end of pumping 45 minutes 15 minutes 26:28 30 minutes PUMPING TEST 60 feet 60 3 Steet 53feet 60 70 ☐ Cloudy GPM Recommended pump rate 43-45 pump setting Deep Shallow 70 GPM CR# 10 FINAL SPATUS OF WELL

Water supply

Observation well

Test hole

Pecharge well Abandoned, insufficient supply a Unfinished Abandoned, poor quality Beplacement well Abandoned (Other) , Dewatering WATER USE 5 Commercial
6 Municipal
7 Public supply
8 Cooling & air conditioning □ Not used
□ Other VISTA RD Domestic Stock Irrigation APPROX Industrial METHOD OF CONSTRUCTION 57 9 Driving
10 Digging
11 Other Cable tool
Rotary (conventional)
Rotary (reverse)
Rotary (air) 5 Air percussion
6 Boring
7 Diamond
8 Jetting 166476 Well Contractor's Licence No Name of Well Contractor Data source 3367 FEB 2 6 1997 Herb Lang Well Drilling Ltd. Date of inspection USE R.R. #1 Omemee, Ontario Well Technician's Licence No. Name of Well Technician Remarks MINISTRY T = 0231Dave Fisher of Tenhician/Conf CSS. S 0506 (07/94) Front Form 9

2 - MINISTRY OF ANVIRONMENT & ENERGY COPY



Print only in spaces provided. 5117898 Mark correct box with a checkmark, where applicable CON PETERBOROUGH Township/Borough/City/Town/Village Con block tract survey, etc. County or District 8 Peterboro 09,1998 KOLIVU Date completed 03 Basin Code 31 18 24 21 LOG OF OVERBURDEN AND BEDROCK MATERIALS (see instructions) Depth - feet General description Other materials Most common material General colour From 0-22 0-21 Cemented Tile Joint's 10 CASING & OPEN HOLE RECORD Sizes of opening (Slot No.) WATER RECORD Inside diam inches Depth - feet Wall thickness SCREEN Water found at - feet inches feet Material Kind of water From То inches Depth at top of screen 30 Material and type 0, 2 2 | Salty | Gas a 2 Steel
Galvanized
Concrete
Open hole
Plastic 30 0 1 Fresh 3 Sulphur 4 Minerals 2 Gas **PLUGGING & SEALING RECORD** 20-23 Steel 19
Galvanized
Concrete
Open hole
Plastic ☐ Annular space 1 Fresh 3 Sulphur 4 Minerals 5 Gas Depth set at - feet Material and type (Cement grout, bentonite, etc.) From Steel
Galva
Concr 18-21 22-25 Galvanized Concrete Open hole Plastic Sulphur Minerals Gas 26-29 Duration of pumping3.... Hours ... LOCATION OF WELL Pumping test method
Pump 2 Bailer Pumping rate 25 GPM In diagram below show distances of well from road and lot line. Indicate north by arrow. Water level end of pumping 1 [] Pumping Static level 45 minutes 32-34 19-21 15 minutes 30 minutes 29-31 60 minutes 0. 1835-37 0 22 019 0-18 0 18 0 - 18 feet feet PUMPING Pump intake set at Water at end of test If flowing give rate O - 20 Recommended pump setting ☐ Cloudy GPM Clear Norm Recommended Recommended pump type pump rate Shallow Deep 0-20 GPM FINAL STATUS OF WELL s | Abandoned, insufficient supply • | Unfinished
• | Abandoned, poor quality to | Replacement well
7 | Abandoned (Other)
8 | Dewaltering Water supply
Description well
Description
Test hole
Description 55-56 WATER USE 9 🗌 Not used 10 🗎 Other Domestic Domestic District Dis

METHOD OF CONSTRUCTION	Priving Digging Digging Other
Name of Well Contractor RIChurd Lott	Well Contractor's Licence No.
Address Survey Dr Oshawa	
Name of Well Technician	Well Technician's Licence No.
Signature of Technician/Contractor	Submission date

4 🔲 Industrial

METHOD OF CONSTRUCTION

ONLY	Data source	Contractor SEP 2 9 1998 00 00 00 00 00 00 00 00 00 00 00 00 00
USE 0	Date of inspection	Inspector
MINISTRY	Remarks	CSS. S9
		0506 (07/94) Front Form 9

187707

Ministry of the Environment

2 - MINISTRY OF THE ENVIRONMENT COPY

Print only in spaces provided.

Mark correct box with a checkmark, where applicable.

5118433

Municipality	Con.		_
51024	COK	1.1	08
4.2	1		

0506 (11/98) Front Form 9

			1 2			*7	14 17		72 - 25 - 25
County or District	,		/Borough/City/T	own/Village			k tract source	y, etc. Lo	t 25:07
Peterbo	rouan	Address	avan				Date		14
		R.R	. #2 O	memee	ontario	C Basin Code	completed	2,4 3	nonth 2 Qua
21	,	ليسبب	Northing	ا ليب	LILLI L	J LILL			Li.
2	19	F OVERBURDEN	N AND BEDR	OCK MAT	ERIALS (see instru	ctions)		,	
General colour	Most common material	Oth	er materials		Gene	ral description		From	r - feet To
Dk. Br.	Top Soil				Loose			0	1
Dk. Br.	Sand	Clay G	ravel		Packed			1	15
Grey	Gravel	Clay S	_	2	Packed			15	36
Grey	Stone	Gtawel			Packed		,	36	57
Grey	Clay	Gravel			Packed			57	108
Grey	Clay				Dense			108	148
Brown	Sand	Clay			Packed			148	164
Grey	Clay	Sand			Packed			164	222
Brown	Gravel Sand	Water			Porous			222	225
~~ ~ # 11	STATEL DAILY	Hatel			101045				- 44:
						1,1-2,-1		1	
31 , , ,	1.1.1.1		Lilili				1,11,,		
32				ـــــا ا					البلنا
	R RECORD 51	~	PEN HOLE P				55 Diameter	34-38 Leng	75 th 39-4
Water found at - feet	Kind of water Inside diam inches	Material	Wall thickness inches	Depth -	To H	ial and type		nches Depth at top	of screen
	Fresh 4	2 Galvanized			13-16	iai and type		Dopur at top	feet
15-18 1 [Fresh 3 Sulphur 19 6-1/	3 ☐ Concrete 4 ☐ Open hole 5 ☐ Plastic	.188	0	225	DI LICCING	& SEALING	DECODE	
20.22	☐ Salty 6 ☐ Gas 17-18 ☐ Fresh 3 ☐ Sulphur 24				20-23 OT	Annular space		Abandonn	
2 [Salty 6 Gas	3 ☐ Concrete 4 ☐ Open hole 5 ☐ Plastic			From 10-13	To Mat	erial and type (Ce	ment grout, b	etc.
ן ז נ	☐ Fresh 3 ☐ Sulphur 29 ☐ Salty 6 ☐ Gas ☐ Salty 6 ☐ Gas			-	27:30 15 0 Holeplu			.g	
30-33	Fresh 3 Sulphur 34 60 4 Minerals Salty 6 Gas	3 Concrete 4 Open hole			26-29	30-33 80			
		5 🔲 Plastic							
71 Pumping test n	. amping.and	Duration of pump Duration of pump Duration of pump Duration of pump Duration of pump Duration of pump Duration of pump	oing 5 . Q.Q . Mins			OCATION OF			4 E
	Water level end of pumping 25 Water levels during		2 ☐ Recovery		In diagram below st Indicate north by ar	row.	or well from t	oad and ic	tine.
19-21	22-24 15 minutes 30 minutes 26-28	\$ 45 minutes 32-34	60 minutes 35-37	l v	WINDY	Acrest	ikm_		
100feet	125 feet 125 feet 125 rate 38-41 Pump intake set at	feet 125 feet Water at epo of te				,			11/1/
Recommended	GPM	feet Clear Recommended	☐ Cloudy 46-49			Hayes L	INK		=}=
Shallow	pump setting 215	pump rate	10 ^{GPM}			- 2.4			
50-53						1400			
FINAL STATU 1 Water sup 2 Observati	pply 5 Abandoned, insufficier	nt suppły ⁹ ☐ Unfinis lity ¹⁰ ☐ Replac	shed	_	,/0	45'	-		
3 ☐ Test hole 4 ☐ Recharge	7 Abandoned (Other)	inty Hepiac	Jement wen	-		CHICKENS	Beau		Ħ
WATER USE	55-56								H
Domestic Stock	Municipal Municipal Monte of the second secon	9 🔲 Not us 10 🔲 Other	e						
 3		ning				•	CR# 10	2	N
	CONSTRUCTION 57					_			
Cable too	onventional) 6 🗆 Boring	9 ☐ Driving 10 ☐ Diggin	g						N .
3 ☐ Rotary (re 4 ☐ Rotary (a	everse) 7 ☐ Diamond sir) 8 ☐ Jetting	Unner	-					217	<u> 361</u>
Name of Well Cont	ractor	Well Contract	tor's Licence No.	→ Data	58 Contracto		59-62 Date rece		63-68
Herb 1	Lang Well Drillin		3367	Source O Date of	<u>.</u>	367	MAY	16 2	000
Address R.R. #1	Odmemee, ontari			Date	of inspection	mspector			
Name of Well Tech	nician	Well Technicia	an's Licence No.		irks		-	~ ~~	
John Lag Signature of Techn		T-2111 Submission d	late	INISTRY Rema				CSS.	ES0
	W //	7-7	<i>~</i>	151					

Ministry of the Environment

Measurements recorded in: Metric Memperial

Well Tag No. (Place Sticker and/or Print Below)

A 147483

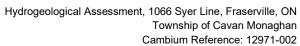
Well Record

Tag#: A147483 Regulation 903 Ontario Water Resources Act

Page_

Address of	f Well Lo	cation (Street Nu	mber/Name)			Township Lot Concession							
0		yer Lin	е			Cavan City/Town/Village Province				8	Б.		
County/Dis		ough				City/Town/Village $egin{array}{ccccc} ext{Province} & ext{Province} & ext{Postal Co} \ ext{Mi} 11brook & ext{O} ext{A} & ext{J} \ ext{O} \ ext{A} & ext{J} \ ext{O} \ ext{A} & ext{J} \ ext{O} \ ext{A} & ext{J} \ ext{A} & ext{J} \ ext{A} \ ext{A} & ext{A} \ ext{A} \ ext{A} & ext{A} \ $							
		one Easting	, No	orthing		Municipal Pl	lan and Subl	ot Number		Other		- 1	
ETHANISM HARMONIA MANAGEMENT	8 3		3 3 4			***************************************						MITOMOTON MAN	954000000000000000000000000000000000000
Overburd General C			ials/Abando non Material			ord (see inst her Material		e back of this form)	al Description			Dec	oth @ /ft)
			non iviateriai			ner Materiai	S	Gener	ai Description		ALPHAN METERS	From	To
Brown	n	C1ay			grave1							0	18
Gray		Clay			layer s	sand						18	56
Gray		Clay									10.00	56	65
Gray		C1ay			gravel			hard			1	65	74
Gray		Limesto	ne							100 Terror Francisco		74	78
											000000000000000000000000000000000000000		
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			www.			***************************************					and the same of th		
D- 11 5	of all real re	1	Annular		-1		DI :		esults of We				
From	et at 🏰 ft To	/	Type of Sea (Material an		u		e Placed 13/ft3)	After test of well yield, w		Time	aw Down Water Level	Time	ecovery Water Level
0	20	Bento	nite s	lurr	у			Other, specify		(min) Static	/ft)	(min)	⟨ (ft)
		dina di La						If pumping discontinued	I, give reason:	Level	14.4		
***************************************										1	16.9	1	23.6
	-			<u> </u>				Pump intake set at m. 55 ft.	/ft)	2	18.6	2	21.0
N # - 41								Pumping rate (1994)	iPM)	3	19.6	3	_
Cable To	-	Construction Diamond	d Put	olic	Well Us		Not used	5 gpm	ŕ	4	20.5	4	17.8
		nal)	Dor		Municip	al 🗆	Dewatering	Duration of pumping 1 hrs + m	in	5	21.1	5	16.8
Rotary (F	Reverse)	☐ Driving ☐ Digging	☐ Irrig		Test Ho	& Air Conditi	Monitoring ioning	Final water level end of		10	22 /	10	1
Air percu			☐ Indi	ustrial er, <i>specii</i>	·			27.0 ft			23.4		15.0
		Construction R			y	Status	of Well	If flowing give rate (I/mi	in / GPM)	15	24.6	15	14.9
Inside	Open I	Hole OR Material	Wall		pth (ft)	Water		Recommended pump	depth 🐗 ft)	20	25.3	20	14.7
Diameter (mylin)	Concre	nized, Fibreglass, te, Plastic, Steel)	Thickness (m/in)	From	То	Replac	ement Well	70 f		25	25.8	25	14.5
$6\frac{1}{4}$ "	Ste	el	.188	+2	74	Rechar	ge Well	Recommended pump		30	26.1	30	14.5
6"	One	nhole		74	78	Dewate Observ	ering Well ation and/or	Well production (I/min /		40	26.6	40	14.4
***************************************	· ·						ing Hole		GFIVI)	50	26.8	50	Les
	<u> </u>			O tely my		(Constr	ruction)	Disinfected? Yes No	10	60	27.0	60	\bigvee
		Construction R	acord - Scree	on.			ient Supply	A Les Mo	Man of We				
Outside		Material			pth (<i>m/ft</i>)	☐ Abando Water (oned, Poor Quality	Please provide a map b	Map of We elow following i	nstructio	ons on the ha	.ck.	
Diameter (cm/in)	(Plastic,	Galvanized, Steel)	Slot No.	From	То	Abando specify	oned, other,	1 4 1		1	15/		
					3 895			100	1 %	71			
					3 3354	Other,	specify	T	*	/	-		
		Water Det	ails		H	ole Diame	ter	10/		800	DI		
		th Kind of Water	_	Untest		h (To	Diameter	1	/_		SyerL		
		as Other, spe th Kind of Water		Untost		20	3"				syer L	120	
		as Other, spe		Jonesia	20	78	6"						
		th Kind of Water		Unteste									
(m.		s Other, spe						10/					
	ame of W	Nell Contracto ell Contractor			We	ion Il Contractor's	Licence No.						
		ons Well		ing	Ltd.	2662		1/m	illBROOK	_			
		treet Number/Nar	,			nicipality	F	Comments:	1,12,100.		7		***************************************
Province	, U , I	42 Count Postal Code	Business			enelor	r Fall	3			1		
ON		KOM 1NO	g har	t@g h	art.ca			Well owner's Date Pac	kage Delivered		Ministr	y Use	Only
	1 1	c. area code) Na		chnician	(Last Name,	First Name)		information package	ty katalo		Audit No.Z	400	2881
705 Well_Technicia	887+ an's Licend	3B31 I	ean J of Technician	im and/or(Contractor Dat	e Submitted		Yes	rk Completed	17			-001
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October 15, 2021

	App	endix	C
AquiferTest	Pro	Resul	lts



194 Sophia St. Peterborough, ON K9H1E5

Pumping Test Analysis Report

Project: Hydrogeological Assessment, 1066 Syer Line, Fraserville, ON

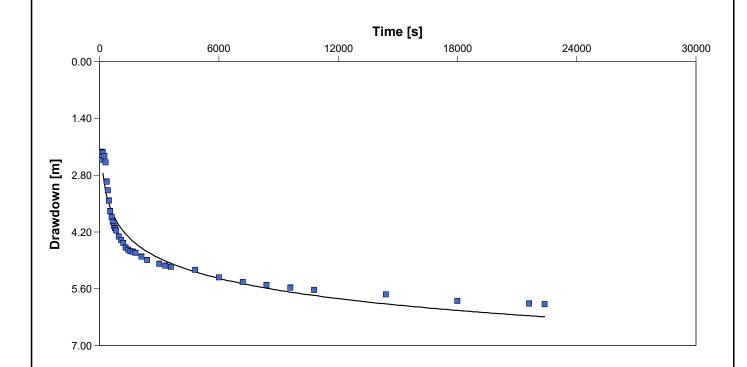
С

Number: 12971-002

Client: Township of Cavan-Monaghan

Location: Fraserville, ON	Pumping Test: Pumping Test 1 - Well 1	Pumping Well: Well 1
Test Conducted by: N. Heikoop		Test Date: 7/19/2021
Analysis Performed by: N. Heikoop	Pump Test - Well 1	Analysis Date: 7/27/2021
		-

Aquifer Thickness: 2.13 m Discharge Rate: 82.5 [U.S. gal/min]



	Calculation using Theis							
Observation Well Transmissivity		Hydraulic Conductivity Storage coefficient		Radial Distance to PW				
		[m²/s]	[m/s]		[m]			
	Well 1	5.75 × 10 ⁻⁴	2.70 × 10 ⁻⁴	8.28 × 10 ⁻¹	0.08			



194 Sophia St. Peterborough, ON K9H1E5

Pumping Test Analysis Report

Project: Hydrogeological Assessment, 1066 Syer Line, Fraserville, ON

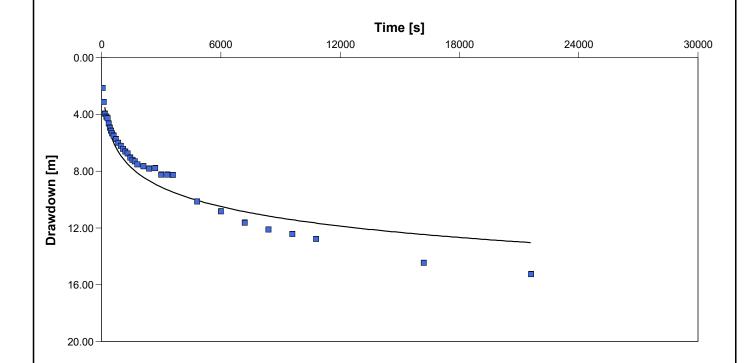
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Number: 12971-002

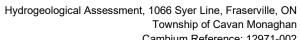
Client: Township of Cavan-Monaghan

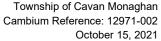
Location: Fraserville, ON	Pumping Test: Pumping Test 1 - Well 2	Pumping Well: Well 2
Test Conducted by: N. Heikoop		Test Date: 7/15/2021
Analysis Performed by: N. Heikoop	Pump Test - Well 2	Analysis Date: 7/27/2021
A :C TI: 1 400	D: 1 D 1 00 010 1/ : 1	

Aquifer Thickness: 4.90 m Discharge Rate: 32 [U.S. gal/min]



Calculation using Theis					
Observation Well	Transmissivity	Hydraulic Conductivity	Storage coefficient	Radial Distance to PW	
	[m²/s]	[m/s]		[m]	
Well 2	8.08 × 10 ⁻⁵	1.65 × 10 ⁻⁵	9.90 × 10 ⁻¹	0.08	







	App	endix D
Laboratory	Water Quality	Results







CA14883-JUL21 R

12971-002, 1066 Syer Line, Fraserville

Prepared for

Cambium Inc.



First Page

CLIENT DETAILS		LABORATORY DETAIL	.s
Client	Cambium Inc.	Project Specialist	Maarit Wolfe, Hon.B.Sc
		Laboratory	SGS Canada Inc.
Address	194 Sofia Street, Peterborough	Address	185 Concession St., Lakefield ON, K0L 2H0
	Canada, K9H 1E3		
	Phone: 705-742-7900. Fax:705-742-7907		
Contact	Mike Bingham	Telephone	705-652-2000
Telephone	705-742-7900	Facsimile	705-652-6365
Facsimile	705-742-7907	Email	
Email	mike.bingham@cambium-inc.com; file@cambium-inc.com	SGS Reference	CA14883-JUL21
Project	12971-002, 1066 Syer Line, Fraserville	Received	07/20/2021
Order Number		Approved	07/27/2021
Samples	Ground Water (2)	Report Number	CA14883-JUL21 R
		Date Reported	07/27/2021

COMMENTS

Temperature of Sample upon Receipt: 10 degrees C

Cooling Agent Present:No Custody Seal Present:No

Chain of Custody Number:025569

SIGNATORIES

Maarit Wolfe, Hon.B.Sc Llwoye

SGS Canada Inc. 185 Concession St., Lakefield ON, K0L 2H0 t 705-652-2000 f 705-652-6365

Member of the SGS Group (SGS SA)

www.sgs.com



TABLE OF CONTENTS

First Page	1
Index	2
Results	3-5
Exceedance Summary	6
QC Summary	7-13
Legend	14
Annexes	15



CA14883-JUL21 R

Client: Cambium Inc.

Project: 12971-002, 1066 Syer Line, Fraserville

Project Manager: Mike Bingham

Samplers: N. Heikosy

PACKAGE:	General	Chemistry	(WATER)
I AOIMAGE.	Jones	OHOHIIGH V	(* * / \

Sample Number

9

Sample Name Well 1

L1 = ODWS_AO_OG / WATER / - - Table 4 - Drinking Water - Reg O.169_03

L2 = ODWS_MAC / WATER / - - Table 1,2 and 3 - Drinking Water - Reg O.169_03

Sample Matrix Ground Water

Sample Date 19/07/2021 L2

Parameter	Units	RL	L1	L2	Result
eneral Chemistry					
Biochemical Oxygen Demand (BOD5)	mg/L	2			< 4↑
Dissolved Oxygen	mg/L	1			10
Total Suspended Solids	mg/L	2			5
Conductivity	uS/cm	2			442
Alkalinity	mg/L as CaCO3	2	500		137
Temperature @ pH	°C	0			18.5
Acidity	mg/L as CaCO3	2			< 2
Total Dissolved Solids	mg/L	30	500		234
Organic Nitrogen	mg/L	0.05	0.15		0.15
Total Kjeldahl Nitrogen (N)	as N mg/L	0.05			0.56
Ammonia+Ammonium (N)	as N mg/L	0.04			0.41
Unionized Ammonia	mg/L as N	0.001			0.020
Hydrogen Sulphide	ug/L	6	50		< 6
Sulphide	μg/L	6			< 6
Dissolved Organic Carbon	mg/L	1	5		1
Total Organic Carbon	mg/L	1			< 1



CA14883-JUL21 R

Client: Cambium Inc.

Project: 12971-002, 1066 Syer Line, Fraserville

Project Manager: Mike Bingham

Samplers: N. Heikosy

Sample Number

9

Result

Sample Name Well 1

.

L1

Sample Matrix Ground Water

L1 = ODWS_AO_OG / WATER / - - Table 4 - Drinking Water - Reg O.169_03
L2 = ODWS_MAC / WATER / - - Table 1,2 and 3 - Drinking Water - Reg O.169_03

Sample Date

RL

Units

mple Date 19/07/2021

Metals and Inorganics

Parameter

letals and Inorganics							
Nitrite (as N)	as N mg/L	0.003			0.003# <mdl< td=""><td></td><td></td></mdl<>		
Nitrate (as N)	as N mg/L	0.006			0.006# <mdl< td=""><td></td><td></td></mdl<>		
Nitrate + Nitrite (as N)	as N mg/L	0.006			0.006# <mdl< td=""><td></td><td></td></mdl<>		
Hardness (dissolved)	mg/L as	0.05	100		113		
	CaCO3						
Aluminum (dissolved)	mg/L	0.001			0.003		
Arsenic (dissolved)	mg/L	0.0002		0.01	< 0.0002		
Barium (dissolved)	mg/L	0.00002		1	0.446		
Boron (dissolved)	mg/L	0.002		5	0.111		
Calcium (dissolved)	mg/L	0.01			23.6		
Cadmium (dissolved)	mg/L	0.00000		0.005	0.000007		
		3					
Chromium (dissolved)	mg/L	0.00008		0.05	< 0.00008	 	
Copper (dissolved)	mg/L	0.0002	1		0.0008		
Iron (dissolved)	mg/L	0.007	0.3		< 0.007		
Sodium (dissolved)	mg/L	0.01	200	20	45.9		
Magnesium (dissolved)	mg/L	0.001			13.1		
Manganese (dissolved)	mg/L	0.00001	0.05		0.00373		
Lead (dissolved)	mg/L	0.00009		0.01	< 0.00009		
Antimony (dissolved)	mg/L	0.0009		0.006	< 0.0009		
Selenium (dissolved)	mg/L	0.00004		0.05	< 0.00004		
Uranium (dissolved)	mg/L	0.00000		0.02	0.000014		
	5, =	2		0.02			
Zinc (dissolved)	mg/L	0.002	5		0.002		
			1				



CA14883-JUL21 R

Client: Cambium Inc.

Project: 12971-002, 1066 Syer Line, Fraserville

Project Manager: Mike Bingham

Samplers: N. Heikosy

PACKAGE: Microbiology (WATER) L1 = ODWS_AO_OG / WATER / Table 4 - Drinking Water - Reg O.169_03 L2 = ODWS_MAC / WATER / Table 1,2 and 3 - Drinking Water - Reg O.169_03				ample Number	9	10
				Sample Name	Well 1	Well 1 Dup
L1 = ODWS_AO_OG / WATER / Table 4 - Drinking Water - Reg O.169_03				Sample Matrix	Ground Water	Ground Water
L1 = ODWS_AO_OG / WATER / Table 4 - Drinking Water - Reg O.169_03 L2 = ODWS_MAC / WATER / Table 1,2 and 3 - Drinking Water - Reg O.169_03 Parameter Units RL Microbiology Total Coliform cfu/100mL 0 E. Coli cfu/100mL 0 Total Coliform Background cfu/100mL 0				Sample Date	19/07/2021	19/07/2021
Parameter	Units	RL	L1	L2	Result	Result
Microbiology						
Total Coliform	cfu/100mL	0		0	0	2
E. Coli	cfu/100mL	0		0	0	0
Total Coliform Background	cfu/100mL	0			540	760
Heterotrophic Plate Count (HPC)	cfu/1mL	0			189	161
Fecal Coliform	cfu/100mL	0			0	0
Other (ORP)						
рН	No unit	5	8.5		8.17	



EXCEEDANCE SUMMARY

Parameter		Method	Units	Result	ODWS_AO_OG / WATER / Table 4 - Drinking Water - Reg O.169_03	ODWS_MAC / WATER / Table 1,2 and 3 - Drinking Water - Reg O.169_03 L2
Well 1						
Hardness (diss	olved)	SM 3030/EPA 200.7	mg/L as CaCO3	113	100	
Sodium (dissolv	ved)	SM 3030/EPA 200.8	mg/L	45.9		20
Well 1 Dup						
Total Coliform		OMOE	cfu/100mL	2		0

				_	
Total Coliform	OMOE	cfu/100mL	2		0
	MICROMFDC-E3407A				

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QC SUMMARY

Acidity

Method: SM 2310 | Internal ref.: ME-CA-[ENV]EWL-LAK-AN-006

Parameter	QC batch	Units	RL	Method	Duplicate		LC	S/Spike Blank		Matrix Spike / Ref.		
	Reference			Blank	RPD	AC	Spike	Recovery Limits (%)		Spike Recovery	Recovery Limits	
						(%)	Recovery (%)	Low	High	(%)	Low	High
Acidity	EWL0337-JUL21	mg/L as	2	2	ND	20	98	90	110	NA		
		CaCO3										

Alkalinity

Method: SM 2320 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-006

Parameter	QC batch	Units	RL	Method	Dup	olicate	LC	S/Spike Blank		M	atrix Spike / Re	ef.
	Reference			Blank	RPD	AC	Spike		ery Limits %)	Spike Recovery		ery Limits (%)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Alkalinity	EWL0337-JUL21	mg/L as	2	< 2	0	20	106	80	120	NA		
		CaCO3										

Ammonia by SFA

Method: SM 4500 | Internal ref.: ME-CA-IENVISFA-LAK-AN-007

Parameter	QC batch	Units	RL	Method	Duj	olicate	LC	S/Spike Blank		M	latrix Spike / Ref	ī
	Reference			Blank	RPD	AC	Spike		ery Limits %)	Spike Recovery		ry Limits %)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Ammonia+Ammonium (N)	SKA0220-JUL21	mg/L	0.04	<0.04	ND	10	99	90	110	100	75	125

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QC SUMMARY

Anions by IC

Method: EPA300/MA300-lons1.3 | Internal ref.: ME-CA-[ENV]IC-LAK-AN-001

Parameter	QC batch	Units	RL	Method	Duj	olicate	LC	S/Spike Blank		м	atrix Spike / Ref	i.
	Reference			Blank	RPD	AC	Spike		ry Limits %)	Spike Recovery		ry Limits %)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Nitrate + Nitrite (as N)	DIO0330-JUL21	mg/L	0.006	<0.006	NA		NA			NA		
Nitrite (as N)	DIO0330-JUL21	mg/L	0.003	<0.003	ND	20	96	90	110	83	75	125
Nitrate (as N)	DIO0330-JUL21	mg/L	0.006	<0.006	0	20	106	90	110	91	75	125

Biochemical Oxygen Demand

Method: SM 5210 | Internal ref.: ME-CA-[ENV]EWL-LAK-AN-007

Parameter	QC batch	Units	RL	Method	Duj	olicate	LC	S/Spike Blank		M	latrix Spike / Ref	·.
Reference	Reference			Blank	RPD	AC	Spike		ry Limits %)	Spike Recovery		ry Limits %)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Biochemical Oxygen Demand (BOD5)	BOD0035-JUL21	mg/L	2	< 2	14	30	101	70	130	NV	70	130

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QC SUMMARY

Carbon by SFA

Method: SM 5310 | Internal ref.: ME-CA-[ENV]SFA-LAK-AN-009

Parameter	QC batch	Units	RL	Method	Dup	licate	LC	S/Spike Blank		M	latrix Spike / Re	f.
	Reference			Blank	RPD	AC	Spike	Recove	-	Spike Recovery		ory Limits %)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Dissolved Organic Carbon	SKA0236-JUL21	mg/L	1	<1	1	10	93	90	110	109	75	125
Total Organic Carbon	SKA0236-JUL21	mg/L	1	<1	1	10	93	90	110	109	75	125

Conductivity

Method: SM 2510 | Internal ref.: ME-CA-[ENV]EWL-LAK-AN-006

Parameter	QC batch	Units	RL	Method	Dup	olicate	LC	S/Spike Blank		м	atrix Spike / Re	ıf.
	Reference			Blank	RPD	AC (%)	Spike		ry Limits %)	Spike Recovery		ery Limits %)
				(%)	Recovery (%)	Low	High	(%)	Low	High		
Conductivity	EWL0337-JUL21	uS/cm	2	< 2	0	20	98	90	110	NA		

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QC SUMMARY

Metals in aqueous samples - ICP-MS

Method: SM 3030/EPA 200.8 | Internal ref.: ME-CA-[ENVISPE-LAK-AN-006

Parameter	QC batch	Units	RL	Method	Dup	licate	LC	S/Spike Blank		Ma	atrix Spike / Ref	f.
	Reference			Blank	RPD	AC (%)	Spike Recovery	Recove	•	Spike Recovery		ery Limits %)
						(7.5)	(%)	Low	High	(%)	Low	High
Aluminum (dissolved)	EMS0147-JUL21	mg/L	0.001	<0.001	6	20	94	90	110	103	70	130
Arsenic (dissolved)	EMS0147-JUL21	mg/L	0.0002	<0.0002	5	20	100	90	110	115	70	130
Barium (dissolved)	EMS0147-JUL21	mg/L	0.00002	<0.00002	1	20	93	90	110	93	70	130
Boron (dissolved)	EMS0147-JUL21	mg/L	0.002	<0.002	5	20	100	90	110	92	70	130
Calcium (dissolved)	EMS0147-JUL21	mg/L	0.01	<0.01	4	20	97	90	110	99	70	130
Cadmium (dissolved)	EMS0147-JUL21	mg/L	0.000003	<0.000003	10	20	98	90	110	97	70	130
Chromium (dissolved)	EMS0147-JUL21	mg/L	0.00008	<0.00008	ND	20	97	90	110	95	70	130
Copper (dissolved)	EMS0147-JUL21	mg/L	0.0002	<0.0002	ND	20	95	90	110	90	70	130
Iron (dissolved)	EMS0147-JUL21	mg/L	0.007	<0.007	5	20	99	90	110	100	70	130
Magnesium (dissolved)	EMS0147-JUL21	mg/L	0.001	0.001	6	20	102	90	110	96	70	130
Manganese (dissolved)	EMS0147-JUL21	mg/L	0.00001	<0.00001	3	20	99	90	110	99	70	130
Sodium (dissolved)	EMS0147-JUL21	mg/L	0.01	<0.01	9	20	102	90	110	98	70	130
Lead (dissolved)	EMS0147-JUL21	mg/L	0.00009	<0.00001	1	20	100	90	110	108	70	130
Antimony (dissolved)	EMS0147-JUL21	mg/L	0.0009	<0.0009	ND	20	100	90	110	101	70	130
Selenium (dissolved)	EMS0147-JUL21	mg/L	0.00004	<0.00004	3	20	103	90	110	99	70	130
Uranium (dissolved)	EMS0147-JUL21	mg/L	0.000002	<0.000002	6	20	95	90	110	84	70	130
Zinc (dissolved)	EMS0147-JUL21	mg/L	0.002	<0.002	5	20	97	90	110	98	70	130

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QC SUMMARY

Microbiology

Method: OMOE MICROMFDC-E3407A | Internal ref.: ME-CA-[ENV]MIC-LAK-AN-001

Parameter	QC batch	Units	RL	Method	Dupl	icate	LC	S/Spike Blank		М	atrix Spike / Ref	
	Reference			Blank	RPD	AC	Spike		ery Limits %)	Spike Recovery	Recover	•
						(%)	Recovery (%)	Low	High	(%)	Low	High
Total Coliform Background	BAC9332-JUL21	cfu/100mL	-	ACCEPTED	ACCEPTE							
					D							
E. Coli	BAC9332-JUL21	cfu/100mL	-	ACCEPTED	ACCEPTE							
					D							
Fecal Coliform	BAC9332-JUL21	cfu/100mL	-	ACCEPTED	ACCEPTE							
					D							
Heterotrophic Plate Count (HPC)	BAC9332-JUL21	cfu/1mL	-	ACCEPTED	ACCEPTE							
					D							
Total Coliform	BAC9332-JUL21	cfu/100mL	-	ACCEPTED	ACCEPTE							
					D							

рΗ

Method: SM 4500 | Internal ref.: ME-CA-[ENV]EWL-LAK-AN-006

Parameter	QC batch	Units	RL	Method	Dup	licate	LC	S/Spike Blank		м	atrix Spike / Ref	
	Reference			Blank	RPD	AC (%)	Spike		ery Limits %)	Spike Recovery	Recover	•
						(%)	Recovery (%)	Low	High	(%)	Low	High
рН	EWL0337-JUL21	No unit	5	NA	0		101			NA		

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QC SUMMARY

Solids Analysis

Method: SM 2540C | Internal ref.: ME-CA-[ENV]EWL-LAK-AN-005

Parameter	QC batch	Units	RL	Method	Duj	plicate	LC	S/Spike Blank		M	latrix Spike / Ref	:
	Reference			Blank	RPD	AC	Spike		ry Limits %)	Spike Recovery		ry Limits %)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Total Dissolved Solids	EWL0323-JUL21	mg/L	30	<30	ND	20	98	90	110	NA		

Sulphide by SFA

Method: SM 4500 | Internal ref.: ME-CA-IENVISFA-LAK-AN-008

Parameter	QC batch	Units	RL	Method	Dup	plicate	LC	S/Spike Blank		м	atrix Spike / Ref	f.
	Reference			Blank	RPD	AC	Spike		ry Limits %)	Spike Recovery		ery Limits
						(%)	Recovery (%)	Low	High	(%)	Low	High
Sulphide	SKA0221-JUL21	ug/L	6	<0.006	ND	20	88	80	120	NA	75	125

Suspended Solids

Method: SM 2540D | Internal ref.: ME-CA-[ENV]EWL-LAK-AN-004

Parameter	QC batch	Units	RL	Method	Duj	olicate	LC	S/Spike Blank		M	atrix Spike / Ref	1
	Reference			Blank	RPD	AC	Spike		ry Limits %)	Spike Recovery	Recover	-
						(%)	Recovery (%)	Low	High	(%)	Low	High
Total Suspended Solids	EWL0367-JUL21	mg/L	2	< 2	2	10	100	90	110	NA		

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QC SUMMARY

Total Nitrogen

Method: SM 4500-N C/4500-NO3- F | Internal ref.: ME-CA-IENVISFA-LAK-AN-002

Parameter	QC batch	Units	RL	Method	Dup	licate	LC	S/Spike Blank		M	latrix Spike / Ref	
	Reference			Blank	RPD	AC (%)	Spike		ry Limits %)	Spike Recovery	Recove	-
						(%)	Recovery (%)	Low	High	(%)	Low	High
Total Kjeldahl Nitrogen (N)	SKA0219-JUL21	mg/L	0.05	<0.05	1	10	102	90	110	102	75	125

Method Blank: a blank matrix that is carried through the entire analytical procedure. Used to assess laboratory contamination.

Duplicate: Paired analysis of a separate portion of the same sample that is carried through the entire analytical procedure. Used to evaluate measurement precision.

LCS/Spike Blank: Laboratory control sample or spike blank refer to a blank matrix to which a known amount of analyte has been added. Used to evaluate analyte recovery and laboratory accuracy without sample matrix effects.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate laboratory accuracy with sample matrix effects.

Reference Material: a material or substance matrix matched to the samples that contains a known amount of the analyte of interest. A reference material may be used in place of a matrix spike.

RL: Reporting limit

RPD: Relative percent difference

AC: Acceptance criteria

Multielement Scan Qualifier: as the number of analytes in a scan increases, so does the chance of a limit exceedance by random chance as opposed to a real method problem. Thus, in multielement scans, for the LCS and matrix spike, up to 10% of the analytes may exceed the quoted limits by up to 10% absolute and the spike is considered acceptable.

Duplicate Qualifier: for duplicates as the measured result approaches the RL, the uncertainty associated with the value increases dramatically, thus duplicate acceptance limits apply only where the average of the two duplicates is greater than five times the RL. **Matrix Spike Qualifier**: for matrix spikes, as the concentration of the native analyte increases, the uncertainty of the matrix spike recovery increases. Thus, the matrix spike acceptance limits apply only when the concentration of the matrix spike is greater than or equal to the concentration of the native analyte.

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LEGEND

FOOTNOTES

NSS Insufficient sample for analysis.

RL Reporting Limit.

- † Reporting limit raised.
- ↓ Reporting limit lowered.
- NA The sample was not analysed for this analyte
- ND Non Detect

Samples analysed as received. Solid samples expressed on a dry weight basis. "Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples.

Analysis conducted on samples submitted pursuant to or as part of Reg. 153/04, are in accordance to the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act" published by the Ministry and dated March 9, 2004 as amended.

SGS provides criteria information (such as regulatory or guideline limits and summary of limit exceedances) as a service. Every attempt is made to ensure the criteria information in this report is accurate and current, however, it is not guaranteed. Comparison to the most current criteria is the responsibility of the client and SGS assumes no responsibility for the accuracy of the criteria levels indicated. This document is issued, on the Client's behalf, by the Company under its General Conditions of Service available on request and accessible at http://www.sgs.com/terms_and_conditions.htm. The Client's attention is drawn to the limitation of liability, indemnification and jurisdiction issues defined therein. Any other holder of this document is advised that information contained hereon reflects the Company's findings at the time of its intervention only and within the limits of Client's instructions, if any. The Company's sole responsibility is to its Client and this document does not exonerate parties to a transaction from exercising all their rights and obligations under the transaction documents.

This report must not be reproduced, except in full. This report supersedes all previous versions.

-- End of Analytical Report --

20210727 14 / 15

Contact Mike Bingham Address: 194 Sophia Company:__ Received Time: Received Date: Received By: referborough KAHIES Address: Kequest for Laboratory Services and CHAIN OF CUSTO.

Environment, Health & Safety - Lakefield: 185 Concession St., Lakefield, ON KOL 2H0 Phone: 705-652-2000 Fax: 705-652-6365 Web: www.sgs.com/environment mike + birghame

Combiner int ion Email: REPORT INFORMATION 00pt the 30t annbium Inc. (hr:min) (mm/dd/yy) SAHAM Received By (signature): -London: 657 Consortium Court, London, ON, N6E 2S8 Phone: 519-672-4500 Toll Free: 877-848-8060 Fax: 519-672-0361 Phone: Contact: Company: (same as Report Information) INVOICE INFORMATION Custody Seal Intact: Yes Custody Seal Present: Yes Request for Laboratory Services and CHAIN OF CUSTODY Laboratory Information Section - Lab use only ₹ ₹ **(** PLEASE CONFIRM RUSH FEASIBILITY WITH SGS REPRESENTATIVE PRIOR TO SUBMISSION RUSH TAT (Additional Charges May Apply): Specify Due Date: Project #: Quotation #: Regular TAT (5-7days) Cooling Agent Present: Yes \(\text{No} \) No \(\text{No} \) Type:\(\text{Temperature Upon Receipt ("C)} \) \(\text{LO} \) \(\text{LO} \) \(\text{LO} \). 20011575 2021 952 *NOTE: DRINKING (POTABLE) WATER SAMPLES FOR HUMAN CONSUMPTION MUST BE SUBMITTED TURNAROUND TIME (TAT) REQUIRED 1 Day 2 Days 3 Days 4 Days WITH SGS DRINKING WATER CHAIN OF CUSTODY Samples received after 6pm or on weekends: TAT begins next business day TAT's are quoted in business days (exclude statutory holidays & weekends). P.O. #: Site Location/ID: 1066 Syer Line, Frage will a Ok LABLIMS# CANYSES-Page N:025569 たえや

REGI	REGULATIONS								ANALYSIS REQUESTED	LYSI	SRI	U	EST	ED						
O.Reg 153/04 O.Reg 406/19	Other Regulations:	ons:	Sewer	Sewer By-Law:	M &	-	SVOC	P	CB PI	PHC	VOC		Pest		ther	(please	Other (please specify)	SPLP TCLP	두	
Res/Park	Reg 347/558 (3 Day min TAT)	(3 Day min TA		Sanitary														Specify Spe	Specify	
Table 2 Ind/Com Coarse	□ PWQ0 □	MMER		Storm		1"		П							_				tests	
Table 3 Agri/Other Medium/Fine	CCME	Other:	Munic	Municipality:)			lor								W	3			
Table Appx.	MISA	rounds	-		R-soil			Aroc								4	Pkg	Owedate O	D _{we}	
Soil Volume	ODWS Not Reportable *See note	eportable *See	note		ics C,SAF		Mo,Ni							te	m					COMMENTS
RECORD OF SITE CONDITION (RSC)	☐ YES ☐	NO			gan ws),eo	y	Cu,Pb,I						-	10	7 <u>0</u>	-	rizat		D VOC	COMMENT OF
	1		5		& Inor	als on	ily	BNs, CPs		ity			e or speci	rai	fer filte		aracte	- 8	□B(a)p	
SAMPLE IDENTIFICATION	SAMPLED	SAMPLED	# OF BOTTLES	MATRIX	Field Filt Metals & incl CrVI, CN,H (CI, Na-water)	Full Met	PAHs on	SVOCs all incl PAHs, Al	F1-F4 +	F1-F4 on	VOCs all incl BTEX	BTEX onl	Organochlorine	Aspe	Bac	Las	Sewer Us Specify pkg: Water Ch General		□ _{ABN}	
1 Well 1	DAI191/a	3535	-								-			12	×	-				
2 Wey Dup	07/19/21	36.50	υ								-		-		7	+				
3						E++					_			-	-	-				
4						120-470					-			-	-	+				
S						(7-10)					\vdash		-	╁	+	+			-	
6						874					-			-	-	╁				
7						giri-n					_			-		\vdash			-	
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Observations/Comments/Special Instructions	なりま	on al	almoot	105	metals)	Las	herery	-	Bothe	1		C A						2		
Sampled By (NAME): N. HELLOS			Signature:	Mar	PK	1/					0	Date: 5	277	20	12	2021	(mm/dd/yy)	3)	Pi	Pink Copy - Client
Relinquished by (NAME): Myke & ngkow	7		Signature:	m				3				Date: 5	2	9	12	12021	(mm/dd/yy)	y)	Ye Ye	Yellow & White Copy - SGS
Note: Submission of sample's to SGS is acknowledgement that you have been provided direction on sample collection and sample collection and instruction of sample's to SGS is acknowledgement that you have been provided direction on sample collection of samples. (2) acknowledgement to some of sample's to SGS is acknowledgement that you have been provided direction of sample collection of sample's to SGS is acknowledgement that you have been provided direction of sample's to SGS is acknowledgement that you have been provided direction of sample's to SGS is acknowledgement that you have been provided direction of sample's to SGS is acknowledgement that you have been provided direction of sample's to SGS is acknowledgement that you have been provided direction of sample's to SGS is acknowledgement that you have been provided direction of sample's to SGS is acknowledgement that you have been provided direction of sample's to SGS is acknowledgement that you have been provided direction of sample's to SGS is acknowledgement that you have been provided direction of sample of SGS is acknowledgement that you have been provided direction of sample's to SGS is acknowledgement that you have been provided direction of sample of SGS is acknowledgement that you have been provided direction of sample of SGS is acknowledgement to sample of SGS is acknowledgem	is acknowledgement that the format (e.g. shipping http://x	t you have been documents). {3} www.sgs.com/ten	Results may be ms_and_conditi	sent by email to ons.htm. (Printe	in that you have been provided direction on sample collectioninationing and increptation of samples, (2) but have been provided direction on sample collectioninations in the first print documents). (3) Results may be sent by email to an unlimited number of addresses for no additional cost. Fax is available upon request. This document is issued by the Company under print	per of address	ses for no a	idditional contion is draw	n to the lin	available nitation of	upon req	luest. Th	is docur	nent is it	ssued by liction is	the Cor	mpany under its G fined therein.	eneral Conditi	tions of S	uninsball to satisfies to 300 is considered administration for company or the "organization of popular or the format of the control of the co







CA14139-JUL21 R

12971-001, 1066 Syer Line, Fraserville ON

Prepared for

Cambium Inc.





First Page

CLIENT DETAILS	S	LABORATORY DETAI	LS
Client	Cambium Inc.	Project Specialist	Jill Campbell, B.Sc.,GISAS
		Laboratory	SGS Canada Inc.
Address	194 Sofia Street	Address	185 Concession St., Lakefield ON, K0L 2H0
	Peterborough, ON		
	K9H 1E3. Canada		
Contact	Mike Bingham	Telephone	2165
Telephone	705-742-7900	Facsimile	705-652-6365
Facsimile	705-742-7907	Email	jill.campbell@sgs.com
Email	mike.bingham@cambium-inc.com; file@cambium-inc.com	SGS Reference	CA14139-JUL21
Project	12971-001, 1066 Syer Line, Fraserville ON	Received	07/14/2021
Order Number		Approved	07/21/2021
Samples	Ground Water (2)	Report Number	CA14139-JUL21 R
		Date Reported	07/21/2021

COMMENTS

MAC - Maximum Acceptable Concentration

AO/OG - Aesthetic Objective / Operational Guideline

MDL - SGS Method Detection Limit

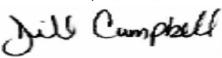
Dioxins/Furans - sub-contracted to Wellington Laboratories.

Radionuclides - sub-contracted to Bequerel Laboratories.

Note: Cyanide reported as total cyanide. The total cyanide incorporates all species of cyanide including free cyanide.

SIGNATORIES

Jill Campbell, B.Sc.,GISAS



t 2165

www.sgs.com



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Annexes	16



CA14139-JUL21 R

Client: Cambium Inc.

Project: 12971-001, 1066 Syer Line, Fraserville ON

Project Manager: Mike Bingham

Samplers: N. Heikosy

PACKAGE:	General	Chemistry	(WATER)

Sample Number

L1

9

Result

Sample Name Well 2

L1 = ODWS_AO_OG / WATER / - - Table 4 - Drinking Water - Reg O.169_03

Sample Matrix Ground Water

L2 = ODWS_MAC / WATER / - - Table 1,2 and 3 - Drinking Water - Reg O.169_03

Units

RL

L2

Sample Date 14/07/2021

General	Chemistry	

Parameter

	0	• • •		
eneral Chemistry				
Biochemical Oxygen Demand (BOD5)	mg/L	2		< 4↑
Dissolved Oxygen	mg/L	1		5.3
Total Suspended Solids	mg/L	2		269
Conductivity	uS/cm	2		373
Alkalinity	mg/L as CaCO3	2	500	206
Temperature @ pH	°C	0		19.2
Acidity	mg/L as CaCO3	2		< 2
Total Dissolved Solids	mg/L	30	500	229
Organic Nitrogen	mg/L	0.05	0.15	< 0.05
Total Kjeldahl Nitrogen (N)	as N mg/L	0.05		0.18
Ammonia+Ammonium (N)	as N mg/L	0.04		0.15
Unionized Ammonia	mg/L as N	0.001		0.005
Hydrogen Sulphide	ug/L	6	50	< 6
Sulphide	μg/L	6		< 6
Dissolved Organic Carbon	mg/L	1	5	2
Total Organic Carbon	mg/L	1		1



FINAL REPORT

CA14139-JUL21 R

Client: Cambium Inc.

Project: 12971-001, 1066 Syer Line, Fraserville ON

Project Manager: Mike Bingham

Samplers: N. Heikosy

ACKAGE: Metals and Inorganics (WATE	=D)		San	nple Number	9
MOIMOL. INICIAIS AIIU IIIUI YAIIUS (WATE	-11)			ample Name	Well 2
= ODWS_AO_OG / WATER / Table 4 - Drinking Water - Re	eg O.169 03			ample Matrix	
= ODWS_MAC / WATER / Table 1,2 and 3 - Drinking Wate	-			Sample Date	14/07/2021
Parameter	Units	RL	L1	L2	Result
etals and Inorganics					
Nitrite (as N)	as N mg/L	0.003		1	<0.003
Nitrate (as N)	as N mg/L	0.006		10	<0.006
Nitrate + Nitrite (as N)	as N mg/L	0.006			<0.006
Hardness (dissolved)	mg/L as	0.05	100		167
	CaCO3				
Aluminum (dissolved)	mg/L	0.001			< 0.001
Arsenic (dissolved)	mg/L	0.0002		0.01	< 0.0002
Barium (dissolved)	mg/L	0.00002		1	0.593
Boron (dissolved)	mg/L	0.002		5	0.052
Calcium (dissolved)	mg/L	0.01			40.1
Cadmium (dissolved)	mg/L	0.00000		0.005	< 0.000003
		3			. 0 00000
Chromium (dissolved)	mg/L	0.00008		0.05	< 0.00008
Copper (dissolved)	mg/L	0.0002	1		< 0.0002
Iron (dissolved)	mg/L	0.007	0.3		< 0.007
Sodium (dissolved)	mg/L	0.01	200	20	19.9
Magnesium (dissolved)	mg/L	0.001			16.3
Manganese (dissolved)	mg/L	0.00001	0.05		0.0121
Lead (dissolved)	mg/L	0.00009		0.01	< 0.00009
Antimony (dissolved)	mg/L	0.0009		0.006	< 0.0009
Selenium (dissolved)	mg/L	0.00004		0.05	< 0.00004
Uranium (dissolved)	mg/L	0.00000		0.02	0.000612
Zing (diagelyed)	/I	0.002	5		< 0.002
Zinc (dissolved)	mg/L	0.002	5		► 0.002



CA14139-JUL21 R

Client: Cambium Inc.

Project: 12971-001, 1066 Syer Line, Fraserville ON

Project Manager: Mike Bingham

Samplers: N. Heikosy

PACKAGE: Microbiology (WATER)			Sa	ample Number	9	10
			;	Sample Name	Well 2	Well 2 Dup
L1 = ODWS_AO_OG / WATER / Table 4 - Drinking Wa	ter - Reg O.169_03		;	Sample Matrix	Ground Water	Ground Water
L2 = ODWS_MAC / WATER / Table 1,2 and 3 - Drinkin	g Water - Reg O.169_03			Sample Date	14/07/2021	14/07/2021
Parameter	Units	RL	L1	L2	Result	Result
Microbiology						
Total Coliform	cfu/100mL	0		0	0	0
E. Coli	cfu/100mL	0		0	0	0
Total Coliform Background	cfu/100mL	0			1340	2000
Heterotrophic Plate Count (HPC)	cfu/1mL	0			220	260
Fecal Coliform	cfu/100mL	0			0	0
Other (ORP)						
рН	No unit	5	8.5		7.93	



EXCEEDANCE SUMMARY

ODWS_AO_OG / ODWS_MAC /
WATER / - - Table 4 WATER / - - Table
- Drinking Water - 1,2 and 3 Reg O.169_03 Drinking Water Reg O.169_03
Parameter Method Units Result L1 L2

Well 2

Hardness (dissolved) SM 3030/EPA 200.7 mg/L as CaCO3 167

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QC SUMMARY

Acidity

Method: SM 2310 | Internal ref.: ME-CA-[ENV]EWL-LAK-AN-006

Parameter	QC batch	Units	RL	Method	Dup	olicate	LC	S/Spike Blank		M	atrix Spike / Re	f.
	Reference			Blank	RPD	AC	Spike		ry Limits %)	Spike Recovery		ry Limits %)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Acidity	EWL0269-JUL21	mg/L as	2	3	ND	20	98	90	110	NA		
		CaCO3										

Alkalinity

Method: SM 2320 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-006

Parameter	QC batch	Units	RL	Method	Duj	plicate	LC	S/Spike Blank		M	atrix Spike / Re	ef.
	Reference			Blank	RPD	AC	Spike		ery Limits %)	Spike Recovery		ery Limits (%)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Alkalinity	EWL0269-JUL21	mg/L as	2	< 2	1	20	98	80	120	NA		
		CaCO3										

Ammonia by SFA

Method: SM 4500 | Internal ref.: ME-CA-IENVISFA-LAK-AN-007

Parameter	QC batch	Units	RL	Method	Duj	olicate	LC	S/Spike Blank		M	latrix Spike / Ref	f.
	Reference			Blank	RPD	AC	Spike		ery Limits %)	Spike Recovery		ry Limits %)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Ammonia+Ammonium (N)	SKA0174-JUL21	mg/L	0.04	<0.04	3	10	102	90	110	101	75	125

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QC SUMMARY

Anions by IC

Method: EPA300/MA300-lons1.3 | Internal ref.: ME-CA-[ENV]IC-LAK-AN-001

Parameter	QC batch	Units	RL	Method	Duj	olicate	LC	S/Spike Blank		м	atrix Spike / Ref	
	Reference			Blank	RPD	AC	Spike	Recove	ry Limits %)	Spike Recovery	Recove	ry Limits 6)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Nitrate + Nitrite (as N)	DIO0270-JUL21	mg/L	0.006	<0.006	NA		NA			NA		
Nitrite (as N)	DIO0270-JUL21	mg/L	0.003	<0.003	ND	20	100	90	110	101	75	125
Nitrate (as N)	DIO0270-JUL21	mg/L	0.006	<0.006	0	20	98	90	110	99	75	125

Biochemical Oxygen Demand

Method: SM 5210 | Internal ref.: ME-CA-[ENV]EWL-LAK-AN-007

Parameter	QC batch	Units	RL	Method	Dup	licate	LC	S/Spike Blank		м	atrix Spike / Ref	·.
	Reference			Blank	RPD	AC	Spike	Recove	ry Limits %)	Spike Recovery	Recove	ry Limits %)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Biochemical Oxygen Demand (BOD5)	BOD0025-JUL21	mg/L	2	< 2	5	30	99	70	130	80	70	130

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QC SUMMARY

Carbon by SFA

Method: SM 5310 | Internal ref.: ME-CA-[ENV]SFA-LAK-AN-009

Parameter	QC batch	Units	RL	Method	Dup	licate	LC	S/Spike Blank		M	latrix Spike / Re	f.
	Reference			Blank	RPD	AC	Spike	Recove	ry Limits %)	Spike Recovery		ery Limits %)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Dissolved Organic Carbon	SKA0157-JUL21	mg/L	1	<1	5	10	106	90	110	112	75	125
Total Organic Carbon	SKA0157-JUL21	mg/L	1	<1	5	10	106	90	110	112	75	125

Conductivity

Method: SM 2510 | Internal ref.: ME-CA-[ENV]EWL-LAK-AN-006

Parameter	QC batch	Units	RL	Method	Dup	olicate	LC	S/Spike Blank		M	atrix Spike / Ref	ī
	Reference			Blank	RPD	AC	Spike		ery Limits %)	Spike Recovery	Recove	ry Limits %)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Conductivity	EWL0269-JUL21	uS/cm	2	< 2	3	20	98	90	110	NA		

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QC SUMMARY

Metals in aqueous samples - ICP-MS

Method: SM 3030/EPA 200.8 | Internal ref.: ME-CA-[ENVISPE-LAK-AN-006

Parameter	QC batch	Units	RL	Method	Dup	licate	LC	S/Spike Blank		Ma	atrix Spike / Ref	f.
	Reference			Blank	RPD	AC (%)	Spike Recovery		ry Limits 6)	Spike Recovery		ery Limits %)
						(7.5)	(%)	Low	High	(%)	Low	High
Aluminum (dissolved)	EMS0076-JUL21	mg/L	0.001	<0.001	4	20	105	90	110	111	70	130
Arsenic (dissolved)	EMS0076-JUL21	mg/L	0.0002	<0.0002	2	20	102	90	110	104	70	130
Barium (dissolved)	EMS0076-JUL21	mg/L	0.00002	<0.00002	1	20	103	90	110	102	70	130
Boron (dissolved)	EMS0076-JUL21	mg/L	0.002	<0.002	6	20	105	90	110	109	70	130
Calcium (dissolved)	EMS0076-JUL21	mg/L	0.01	<0.01	1	20	103	90	110	104	70	130
Cadmium (dissolved)	EMS0076-JUL21	mg/L	0.000003	<0.000003	0	20	101	90	110	108	70	130
Chromium (dissolved)	EMS0076-JUL21	mg/L	0.00008	<0.00008	12	20	103	90	110	104	70	130
Copper (dissolved)	EMS0076-JUL21	mg/L	0.0002	<0.0002	12	20	102	90	110	107	70	130
Iron (dissolved)	EMS0076-JUL21	mg/L	0.007	<0.007	0	20	105	90	110	100	70	130
Magnesium (dissolved)	EMS0076-JUL21	mg/L	0.001	<0.001	4	20	107	90	110	104	70	130
Manganese (dissolved)	EMS0076-JUL21	mg/L	0.00001	<0.00001	4	20	103	90	110	104	70	130
Sodium (dissolved)	EMS0076-JUL21	mg/L	0.01	<0.01	5	20	104	90	110	103	70	130
Lead (dissolved)	EMS0076-JUL21	mg/L	0.00009	<0.00001	2	20	108	90	110	108	70	130
Antimony (dissolved)	EMS0076-JUL21	mg/L	0.0009	<0.0009	ND	20	101	90	110	97	70	130
Selenium (dissolved)	EMS0076-JUL21	mg/L	0.00004	<0.00004	3	20	101	90	110	102	70	130
Uranium (dissolved)	EMS0076-JUL21	mg/L	0.000002	<0.000002	2	20	93	90	110	94	70	130
Zinc (dissolved)	EMS0076-JUL21	mg/L	0.002	<0.002	15	20	98	90	110	95	70	130

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QC SUMMARY

Microbiology

Method: OMOE MICROMFDC-E3407A | Internal ref.: ME-CA-[ENV]MIC-LAK-AN-001

Parameter	QC batch	Units	RL	Method	Dupl	icate	LC	S/Spike Blank		M	atrix Spike / Ref	
	Reference			Blank	RPD	AC	Spike		ery Limits %)	Spike Recovery	Recove	ry Limits %)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Total Coliform Background	BAC9274-JUL21	cfu/100mL	-	ACCEPTED	N/A							
E. Coli	BAC9274-JUL21	cfu/100mL	-	ACCEPTED	ACCEPTE							
					D							
Fecal Coliform	BAC9274-JUL21	cfu/100mL	-	ACCEPTED	ACCEPTE							
					D							
Heterotrophic Plate Count (HPC)	BAC9274-JUL21	cfu/1mL	-	ACCEPTED	ACCEPTE							
					D							
Total Coliform	BAC9274-JUL21	cfu/100mL	-	ACCEPTED	ACCEPTE							
					D							

pН

Method: SM 4500 | Internal ref.: ME-CA-[ENVIEWL-LAK-AN-006

Parameter	QC batch	Units	RL	Method	Duj	plicate	LC	S/Spike Blank		M	atrix Spike / Ref	
	Reference			Blank	RPD	AC	Spike	Recove	•	Spike Recovery	Recover	-
						(%)	Recovery (%)	Low	High	(%)	Low	High
рН	EWL0269-JUL21	No unit	5	NA	0		101			NA		

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QC SUMMARY

Solids Analysis

Method: SM 2540C | Internal ref.: ME-CA-[ENV]EWL-LAK-AN-005

Parameter	QC batch	Units	RL	Method	Duj	plicate	LC	S/Spike Blank		M	latrix Spike / Ref	
	Reference			Blank	RPD	AC	Spike		ry Limits %)	Spike Recovery	Recover	ry Limits 6)
						(%)	Recovery (%)	Low	High	(%)	Low	High
Total Dissolved Solids	EWL0254-JUL21	mg/L	30	<30	7	20	96	90	110	NA		

Sulphide by SFA

Method: SM 4500 | Internal ref.: ME-CA-IENVISFA-LAK-AN-008

Parameter	QC batch	Units	RL	Method	Dup	plicate	LC	S/Spike Blank		М	atrix Spike / Ref	f.
	Reference			Blank	RPD	AC	Spike		ry Limits %)	Spike Recovery		ery Limits
						(%)	Recovery (%)	Low	High	(%)	Low	High
Sulphide	SKA0166-JUL21	ug/L	6	<0.006	ND	20	107	80	120	NA	75	125

Suspended Solids

Method: SM 2540D | Internal ref.: ME-CA-[ENV]EWL-LAK-AN-004

Parameter	QC batch	Units	RL	Method	Duj	olicate	LC	S/Spike Blank		M	atrix Spike / Ref	
	Reference			Blank	RPD	AC	Spike		ery Limits %)	Spike Recovery	Recover	-
						(%)	Recovery (%)	Low	High	(%)	Low	High
Total Suspended Solids	EWL0281-JUL21	mg/L	2	< 2	0	10	95	90	110	NA		

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QC SUMMARY

Method Blank: a blank matrix that is carried through the entire analytical procedure. Used to assess laboratory contamination.

Duplicate: Paired analysis of a separate portion of the same sample that is carried through the entire analytical procedure. Used to evaluate measurement precision.

LCS/Spike Blank: Laboratory control sample or spike blank refer to a blank matrix to which a known amount of analyte has been added. Used to evaluate analyte recovery and laboratory accuracy without sample matrix effects.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate laboratory accuracy with sample matrix effects.

Reference Material: a material or substance matrix matched to the samples that contains a known amount of the analyte of interest. A reference material may be used in place of a matrix spike.

RL: Reporting limit

RPD: Relative percent difference

AC: Acceptance criteria

Multielement Scan Qualifier: as the number of analytes in a scan increases, so does the chance of a limit exceedance by random chance as opposed to a real method problem. Thus, in multielement scans, for the LCS and matrix spike, up to 10% of the analytes may exceed the quoted limits by up to 10% absolute and the spike is considered acceptable.

Duplicate Qualifier: for duplicates as the measured result approaches the RL, the uncertainty associated with the value increases dramatically, thus duplicate acceptance limits apply only where the average of the two duplicates is greater than five times the RL.

Matrix Spike Qualifier: for matrix spikes, as the concentration of the native analyte increases, the uncertainty of the matrix spike recovery increases. Thus, the matrix spike acceptance limits apply only when the concentration of the matrix spike is greater than or equal to the concentration of the native analyte.

20210721



LEGEND

FOOTNOTES

NSS Insufficient sample for analysis.

- RL Reporting Limit.
- † Reporting limit raised.
- ↓ Reporting limit lowered.
- NA The sample was not analysed for this analyte
- ND Non Detect

Samples analysed as received. Solid samples expressed on a dry weight basis. "Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples.

Analysis conducted on samples submitted pursuant to or as part of Reg. 153/04, are in accordance to the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act" published by the Ministry and dated March 9, 2004 as amended.

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-- End of Analytical Report --

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